

MARSHALL GRANT
IN-55 PR
102767
188

SEMI-ANNUAL REPORT
DEVELOPMENT OF COMPUTERIZED ANALYSIS FOR
SOLID PROPELLANT COMBUSTION (ISAP-2)

NAG8-627

by

T. J. Chung and Raymond Hallit

Department of Mechanical Engineering
The University of Alabama in Huntsville

prepared for

NASA/MSFC

(NASA-CR-181399) DEVELOPMENT OF
COMPUTERIZED ANALYSIS FOR SOLID PROPELLANT
COMBUSTION (ISAP-2) Semiannual Report
(Alabama Univ.) 78 p Avail: NTIS HC
A05/MF A01

N87-29634

Unclas

CSCL 21B G3/25 0102767

November, 1987

ABSTRACT

This report is an improvement to ISAP-1, "SRB Vorticity-Acoustic Coupled Instability Analysis", September, 1986.

Included in this report are the automatic generation of all input data for grid configuration, boundary conditions for coupled acoustic and vortical field calculations, transformation of all dimensions to a parametric form, resulting in flexibility for the user to define the size of the problem (geometric configurations) with reduction in storage (15-65%) and computer time (50-75%).

Additional research is required for the following areas:

- (1) effects of turbulence, (2) nonlinear wave oscillations, and
- (3) chemistry upon combustion instability.

TABLE OF CONTENTS

	Page
ABSTRACT	i
TABLE OF CONTENTS	ii
LIST OF FIGURES AND TABLES	iii
I. INTRODUCTION	1
II. MESH GENERATION	3
A. Flow Field	3
B. Acoustic and Vortical Field	4
C. Initial and Flow Constants	5
III. PARAMETRIC DIMENSIONS	6
A. Parameters	6
(a) Geometric Parameters	6
(b) Floating Parameter	7
(c) Fixed Parameter	8
B. Arrays	8
IV. COMPARISON OF RESULTS	9
A. Original Grids	10
B. Reduced Grids	11
V. RECOMMENDATIONS	13
A. To the User	13
B. Additional Recommendations	14
APPENDIX - Listing of the Revised Code	23

LIST OF FIGURES AND TABLES

Figure		Page
1.	The grids: a) for the original flow field calculations, b) for the original A/V calculations, c) for the reduced flow calculations, and d) for the reduced A/V calculations.	15
2.	Parameters, boundaries, and domain of calculations.	16
3.	Comparison between the flow field results of the original code and those of the revised code for a) the pressure, b) the U-velocity, and c) the V-velocity; $Re = 10^3$.	17
4.	Comparison of the flow field variables between the original mesh and the reduced mesh: a) the pressure, b) the U-velocity, and c) the V-velocity; $Re = 10^3$.	18
5.	Comparison of the flow field variables between the original mesh and the reduced mesh: a) the pressure, b) the U-velocity, and c) the V-velocity; $Re = 10^4$.	19
6.	Comparison of the flow field variables between the original mesh and the reduced mesh: a) the pressure, b) the U-velocity, and c) the V-velocity; $Re = 10^5$.	20

Tables

1. Comparison of the storage and run time between the original and revised codes at $Re = 10^3$ (original grids). 21
2. The reduced grids. 21
3. Storage and run time comparison between the original and reduced grids (MI was set at 65 as an initial assumption). 22

I. INTRODUCTION

This report represents an improved version of "SRB Vorticity-Acoustic Coupled Instability Analysis - ISAP-1, September, 1986. The many basic changes to the original code include the automatic generation of all the input data for grid structure, boundary conditions, and coupling between the flow field and the acoustic/vortical field. In addition, all the dimensions in the program were transformed into a parametric form. These new parameters will enable the user to control the computer memory storage and the program execution time by specifying different sets of parameters and different geometric configurations. Also presented is the comparison between the results of the original program and those of the new one, along with recommendations to the user and additional research requirements.

As noted in the earlier report (ISAP-1), unstable waves may occur as a result of acoustic and/or vortical (hydrodynamic) oscillations. If these two different types of waves are coupled together, their physical interactions lead to extremely complicated phenomena. Theoretically, there exists an infinite number of frequencies for both acoustic and vortical oscillations. Realistically, however, only a limited number of combined frequencies are excited. Our objective is to determine the combined nature of acoustic and vortical frequencies at which instabilities may arise. This subject is important in rocket motor combustion chambers when the vortical field is coupled with

acoustic pressure oscillations. In the past, the acoustic combustion instability was studied independently of the vortical instability induced by vortex motions. This report is intended to combine the two different sources of energy everywhere within the spatial domain and to determine the effect of one upon the other. This can be achieved by calculating the mean flow velocities and vorticities and their fluctuating parts of velocities and vortices, as well as the fluctuating pressure.

To elucidate this coupling mechanism, the acoustic wave equation and the perturbed vortical transport equation are solved, being combined with the results of mean flow calculations from the Navier-Stokes system by means of finite elements. With these data, growth constants are calculated and stability boundaries determined. Contributions to stability and/or instability from various sources such as combustion, convection (flow turning), and viscous damping on propellant surfaces and energy convection, momentum convection, momentum viscous damping, and dissipative energy from the interior domain are separately identified. It is also found that stability boundaries for coupled acoustic and vortical oscillations are somewhat similar to the classical hydrodynamic stability boundaries, but they occur in the form of multiple islands.

II. MESH GENERATION

In the original version of the program, the input data was read externally, and this procedure required extensive preparation for any changes in the input constants and/or the configuration of the field. This process is complex and time consuming. Consequently, a mesh generation routine is added to the program.

The program has two major parts: (1) the flow field calculations and (2) the acoustic and vortical calculations from which the stability integrals and growth constants are derived. Therefore, a complete set of input data is required for each part.

A. Flow Field

The flow field calculations include velocities and pressure with grid configurations coarser than those in ISAP-1. Figure 1a shows the original grid in ISAP-1. It is apparent that the element sizes are smaller near boundaries (4), (5), and (6) in Fig. 2, but these reductions were set arbitrarily. The mesh generation routine has a much better approach. It reduces the grid size logarithmically near the same boundaries. This will enhance the flexibility of the program. The generated arrays are the following:

- (a) NENN - the element connectivity matrix; it sets the global nodal values of the nodes of each element.
- (b) XX, YY - the coordinates of each global node.

- (c) NU, NV, and ND - the global nodes for the Dirichlet boundary condition adjustment for the U, V velocities and pressure, respectively.
- (d) UB, VB, and PB - the boundary values associated with NU, NV, and ND, respectively.
- (e) UU, VV, PP - the velocities in the x-direction, y-direction, and the pressure, respectively.

B. Acoustic and Vortical Field

This is the smaller grid shown in Fig. 2b,d. The two grids are interconnected through the ICON matrix. Again this connectivity was previously set arbitrarily. While in the mesh generation routine, the new grid is set through ICON, such that the distances between the nodes at each boundary are as equal as possible. The arrays for this field are:

- (a) NENL - the element connectivity matrix for the smaller grid.
- (b) ICON - the interconnectivity matrix between the flow field and the acoustic/vortical field.
- (c) NODE - the adjustment matrix for the boundary conditions in the computation of vortical modes.
- (d) FFX, FFY - the direction cosines at the boundaries in the x and y directions, respectively.
- (e) NBQ - the number of elements at each boundary.
- (f) ABN, ANN - the admittance at the burning surface and nozzle, respectively.
- (g) NC - the connectivity matrix of the boundary elements.

C. Initial and Flow Constants

For each problem, there are some basic constants that are needed to define it. They deal with the geometry, flow properties, error, time-step, and convergence parameters. Many of these constants, such as REN, GAMMA, DT, ERROR, ITMAX, and NPT, have already been defined in the original report. In order to enhance the flexibility of the program, a few additional constants dealing with the geometry of the problem were utilized in the mesh generation routine. They are the following:

- (a) XMIN, XMAX, YMIN, YMAX - the limiting values of the domain.
- (b) X0, Y0 - the coordinates of the corner node (see Fig. 1).

These geometric values must be redefined by the user every time the configuration of the problem changes.

III. PARAMETRIC DIMENSIONS

The original program was bounded by a set of fixed parameters which controls the memory storage requirements. For the flow field, the program used 832 grid points and 767 elements; for the acoustic/vortical field, it used 40 grid points and 27 elements.

In order to make the programs more flexible, parametric dimensions were added. This addition will allow the user to choose the memory storage needed for different executions. This procedure requires the definition of the parameters and the respective arrays.

A. Parameters

A total of 10 parameters is needed to maximize the flexibility of the program. All but two of these parameters are geometric; they will generate both grids. Of the remaining two parameters, one is fixed and the other is floating (not fixed).

(a) Geometric Parameters:

Four parameters are needed for each grid.

1. Flow field:

The four parameters, shown in Fig. 2, are defined as follows:

- NELF1 - the number of boundary elements above the corner node in the y-direction.
- NELF2 - the number of boundary elements below the corner node in the y-direction.

NETP1 - the number of boundary elements left of the corner node in the x-direction.

NETP2 - the number of boundary elements right of the corner node in the x-direction.

2. Acoustic/vortical field:

The four parameters associated with this field are similar to those of the flow field with their respective positions.

NALF1, NALF2, NATP1, and NATP2 are the number of elements on boundaries (5), (1), (6), and (4), respectively (see Fig. 2).

(b) Floating Parameter:

The parameter MI is affected by other parameters and constants and is a direct result of the calculations. In the original code, the value of MI was set at 65. However, this value can be much lower (see Table 3).

From the program, the needed value of MI is augmented for each St (Strouhal number) $\geq .01$. Those values of St $< .01$ will produce oscillations which are negligible relative to the acoustic oscillations and, therefore, are eliminated to avoid unnecessary calculations. As the Reynolds number increases, the vortical oscillations expand further in the field, resulting in higher values of St at additional nodes; therefore, the needed value of MI will increase.

However, in order to limit the memory storage requirements, MI must be minimized. This procedure will be achieved by changing MI relative to the changes in REN and the geometric parameters (see Section V for the recommended values of MI).

(c) Fixed Parameter:

The parameter NBP, which is always equal to 6, represents the 6 boundaries of the domain. It must be noted that the remaining parameters are derived directly from the 10 preset parameters already defined.

B. Arrays

The size of all the different arrays can be set either by a DIMENSION statement or by a COMMON block. When the parameters were added to the program, two other steps had to be taken:

- (1) All the COMMON blocks were eliminated from the code. This step required a change in the way the subroutines are called, by including all the variable arrays that were otherwise included in the COMMON statements.
- (2) All the arrays must be referenced in the MAIN program. This step was required because the dimensions of all the arrays are generated in the PARAMETER statements in the MAIN program.

IV. COMPARISON OF RESULTS

The computer memory storage and the execution time are the important outcome of this study. Therefore, to compare these effects, the results will be displayed in two ways: (1) by comparing the original code and the revised code and (2) by comparing the original grids' results with those of the reduced ones.

First of all, the basic assumptions and flow constants are presented:

1. The Reynolds number, $REN = 10^3, 10^4, 10^5$ for different runs.
2. The specific heat ratio, $GAMMA = 1.2$.
3. The time step for the calculation of the mean flow field, $DT = 1$.
4. The convergence error for mean flow, $ERROR = .001$.
5. The maximum number of iterations for flow field calculations, $ITMAX = 30$.
6. The domain of calculations: $XMIN = 0, XMAX = 10, YMIN = 0, YMAX = 1.5$.
7. The corner node coordinates: $X0 = 2, Y0 = 1$.
8. Boundary and initial conditions: With reference to Fig. 1, burning takes place only on boundary (6); therefore, an instantaneous flux normal to this boundary appears at time $T = 0$. Then, the velocity in the negative y-direction is set at a dimensionless value of $v = -.01$, only at the nodes of boundary (6), and excluding the end points of this boundary. All other flow variables are set equal to zero

everywhere in the domain. (The value of $-.01$ was taken from the original code and is a function of the burning rate at the surface of the solid fuel).

9. The normal vectors at the boundaries: At boundaries (1) - (6), the values of the normal vectors are $FFNX = 1., 0., 1., 0., 1., 0.$; $FFNY = 0., 1., 0., 1., 0., 1.$, respectively.
10. Admittance: Only at the burning surface (boundary 6), $ABN = 1.$; otherwise, it is equal to zero. Only at the nozzle (boundary 3), $AAN = 1.$; otherwise, it is equal to zero.

These assumptions and flow constants were kept fixed (except for REN) throughout the calculations. Now, we can proceed to the comparison of the results.

A. Original Grids

It is clear that with the original grids (ISAP-1), the storage required to generate the data in the revised code will exceed the storage needed to read the data from an outside source. Therefore, the total memory requirements for the revised code exceed that of the original code by about 2%.

Concerning the run time requirements, on the other hand, the revised code used about 2% less time than that of the original code, even though it went through 5 additional values of Strouhal numbers, i.e., vortical calculations (see Table 1).

NOTE: The value of MI has been defined earlier, but this value is also dependent on the systems on which these programs are running. The original code gave a value of $MI = 15$ on the IBM

3084 and a value of $MI = 16$ on the UNIVAC. This phenomenon is a result of the eigenvalue solver routine. This routine is very sensitive to any small variations in its input data. To eliminate the sensitivity problem, these codes should be transformed to operate in double-precision, while reducing the ERROR value and increasing ITMAX. These new additions will increase the storage requirements and run time by over 50%.

The flow field results, as shown in Fig. 3, prove that the revised code presents the same exact flow field as that of the original code. In the figure, the original code results are displayed in the upper half of each section for (a) the pressure, (b) the velocity in the x-direction, and (c) the velocity in the y-direction. These results were expected because of the linearity of the solution. However, the difference between the values of MI was not expected to be as large.

Even though the revised version of the program made it more flexible and easy to operate, it still has not made any major contribution to reduce the memory requirements nor the necessary run time. Therefore, we will present the other aspects of possible improvements which reduce the memory storage and run time. But, as we will see, they will slightly affect the computational results.

B. Reduced Grids

As a part of the flexibility of the revised code, the user has the option of changing the number of nodes and elements used in the program. Figure 1 shows the different grids used for

comparison purposes. The number of nodes and elements are tabulated in Table 2. As seen in Table 2, if the number of elements at the boundaries is reduced by $1/4$, the total number of nodes and elements is reduced by about $1/2$. As a result of the reduced grids, the required memory storage and run time will definitely be reduced. Then, there is a need to find what percentage reduction is achieved and how it will affect the results.

Table 3 shows the different reductions achieved for required memory and run time at different Reynolds numbers. The storage requirement is reduced by 14% and 66% with coarser grids for the flow field and the flow and A/V fields, respectively, while the execution time is reduced between 56% and 76%. From these values, we can conclude that the flow field calculations affect mostly the run time required, while the acoustic/vortical (A/V) field affects the storage size of the program. On the other hand, the computational results of such reductions are slightly affected. Figures 4-6 show the flow field variables for the reduced grid (the lower part of each section), as compared to the original grid, for $Re = 10^3$, 10^4 , and 10^5 , respectively. The difference between the results becomes more obvious as Re gets larger. Consequently, at high values of the Reynolds number (Re), the coarse mesh does not produce accurate results.

V. RECOMMENDATIONS

Two types of recommendations are necessary to conclude this report: (1) those directed towards the users of the program and (2) those needed for a more realistic modeling of the problem at hand.

A. To the user:

- (1) **Grids:** This program does not contain a turbulent flow model to accommodate for the higher values of Re . Also, there is a limit, in reducing the grids, at which the results would become insignificant. Therefore, a coarse mesh, such as (6, 9, 13, 20), may be used at $Re \leq 10^3$; but, at higher values of Re , a more refined mesh is needed. Recommended values for the parameters: $NELF1 \geq 6$, $NELF2 \geq 9$, $NETP1 \geq 13$, $NETP2 \geq 20$, $2 \leq NALF1, NALF2, NATP1, NATP2 \leq 4$. It is imperative that the last 4 parameters be ≥ 2 ; otherwise, the calculations will become senseless.
- (2) **The value of MI:** As stated earlier, the needed value of MI is calculated within the program. The maximum allowable value of MI is equal to the number of A/V modes: $MI_{max} = NT$. In order to control the memory storage requirements, MI can be specified smaller than NT. As shown in Table 3, the needed values of MI increase as the Reynolds number increases.

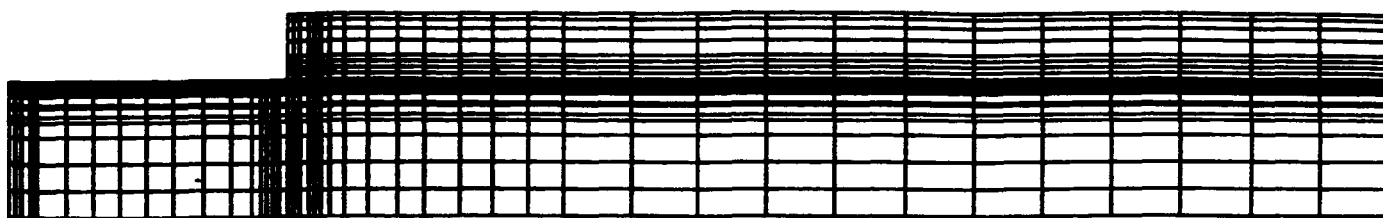
Therefore, it is recommended that the user adjust the value of MI, as needed, to correspond with the values of the Reynolds

number and the appropriate geometric parameters. The recommended values of MI are: $MI_{(needed)} < MI \leq NT$, where $MI_{(needed)}$ are the values listed in Table 3.

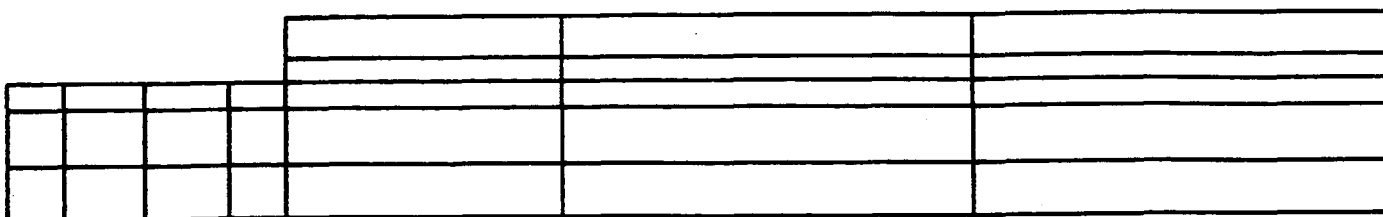
B. Additional Recommendations:

There are many areas where this program can be improved, some of which can be done in the near future, others will be the topics of further study and research.

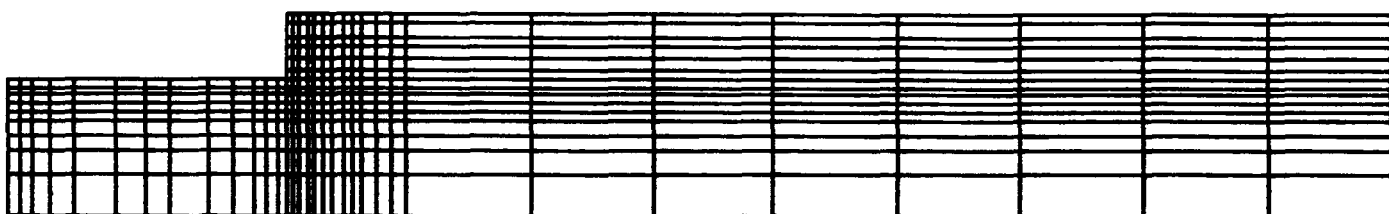
- (1) Double precision, smaller DT, smaller ERROR, and larger ITMAX: these extra steps are needed for accuracy and to avoid the sensitivity in the eigenvalue solver.
- (2) Turbulent model: this model will be used for the relatively high values of Re.
- (3) Higher order approximations of the pressure and the vorticity.
- (4) The study of the effect of compressibility.
- (5) The addition of chemistry to the model by adding the species and energy equations.



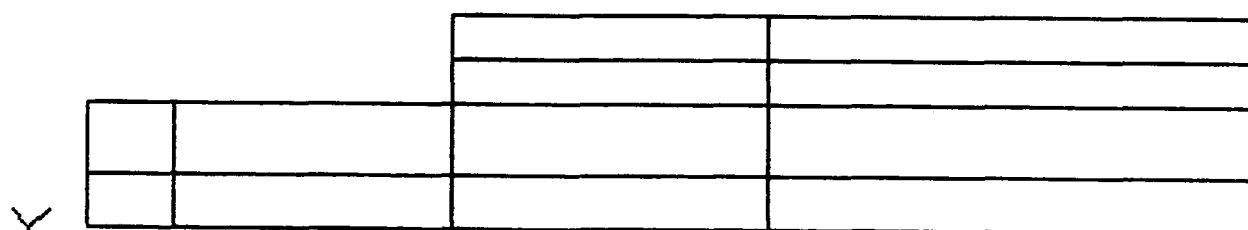
(a)



(b)



(c)



(d)

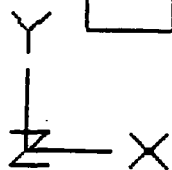


Fig 1. The grids: a) for the original flow calculations, b) for the original A/V calculations, c) for the reduced flow calculations, and d) for the reduced A/V calculations.

NELF1, NALF1
 NELF2, NALF2

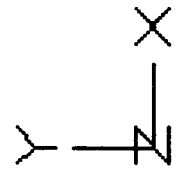
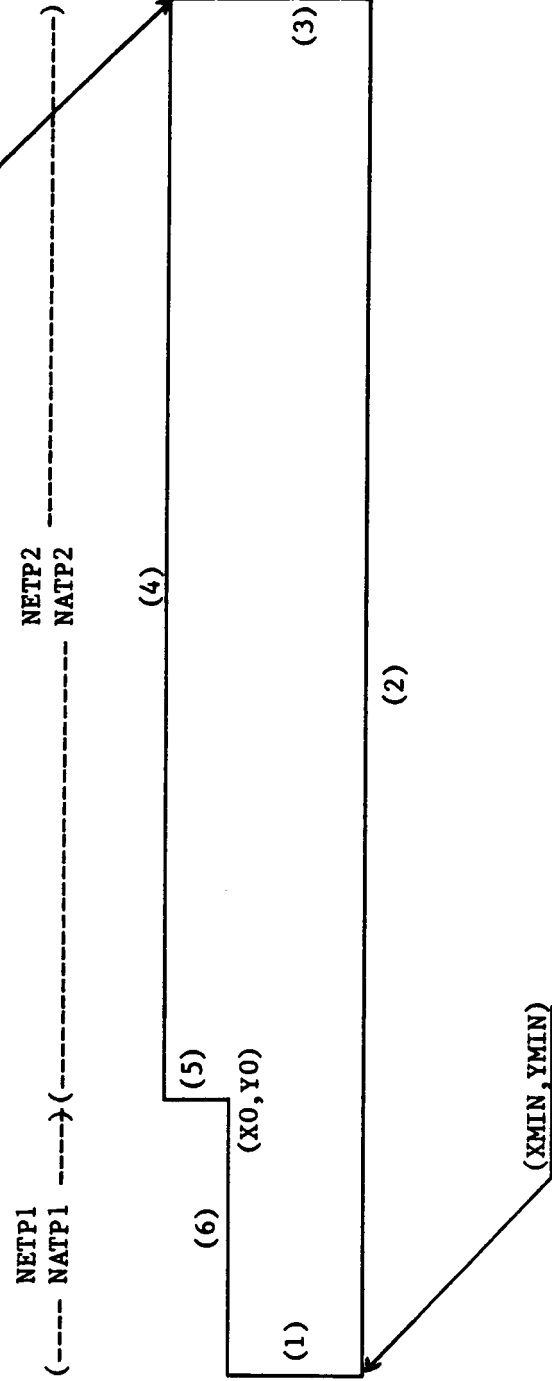
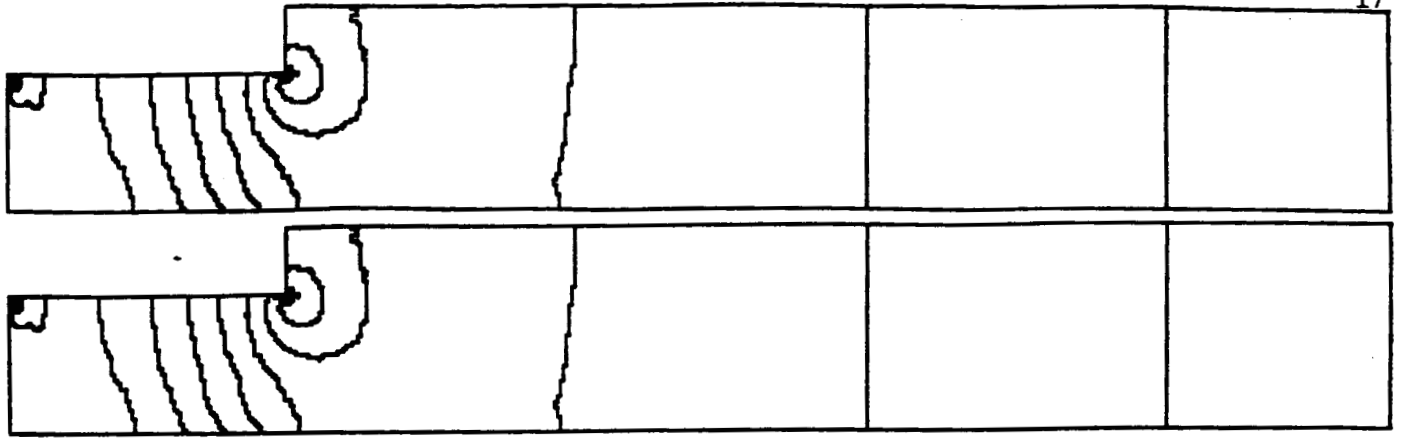
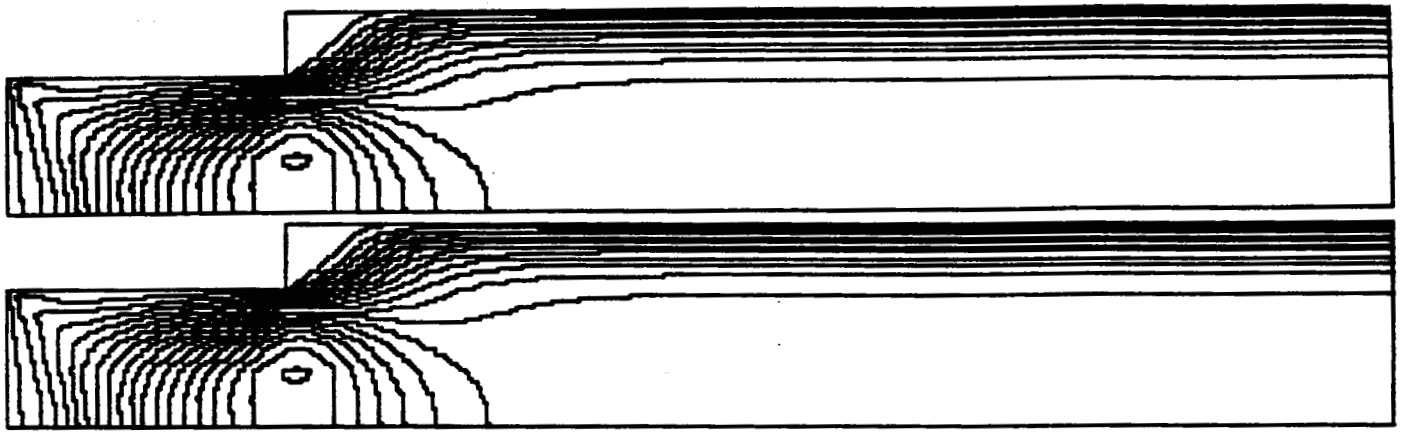


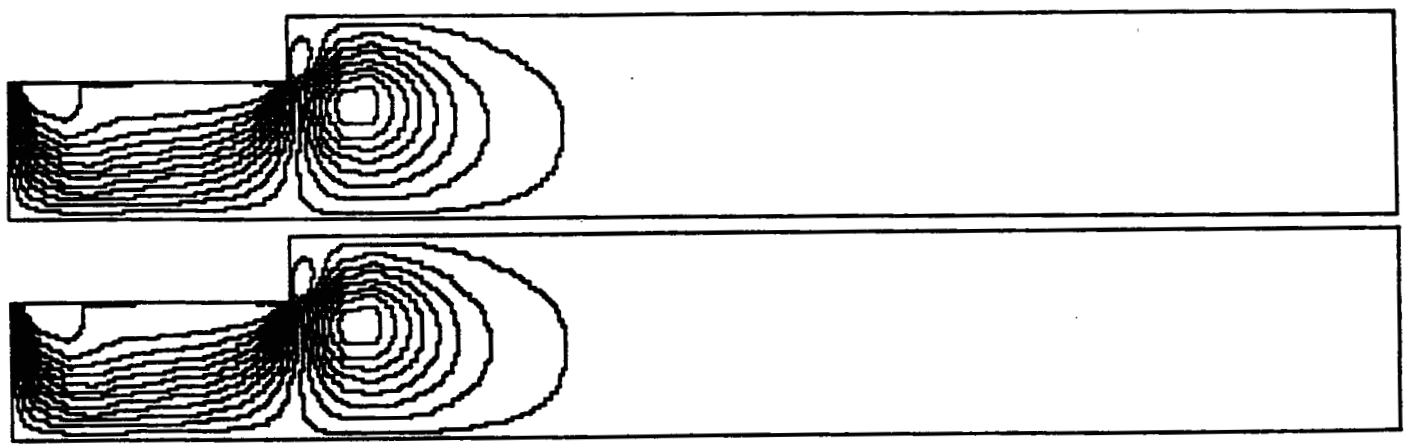
Fig 2. Parameters, boundaries, and domain of calculations.



(a)

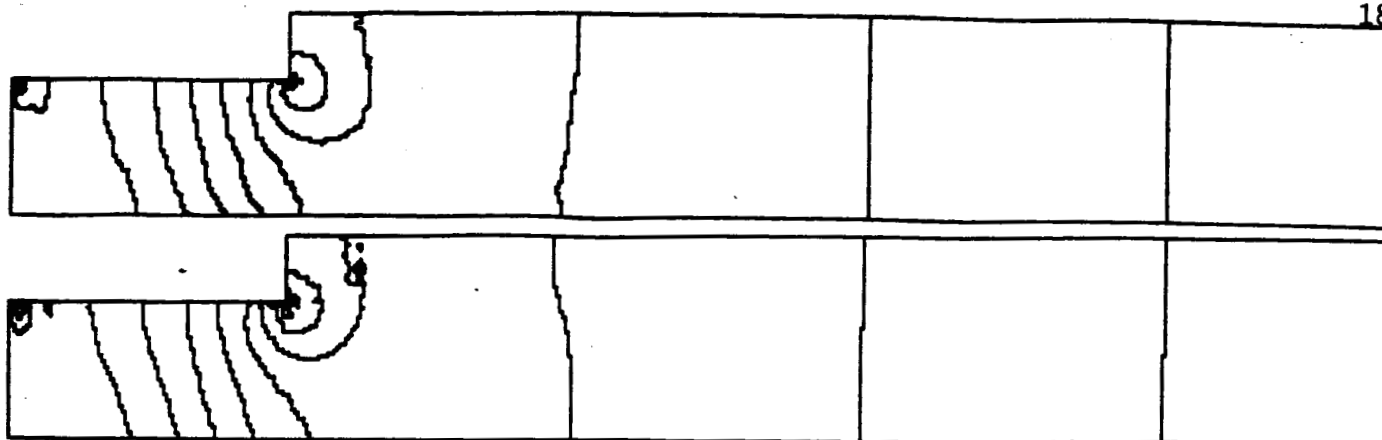


(b)

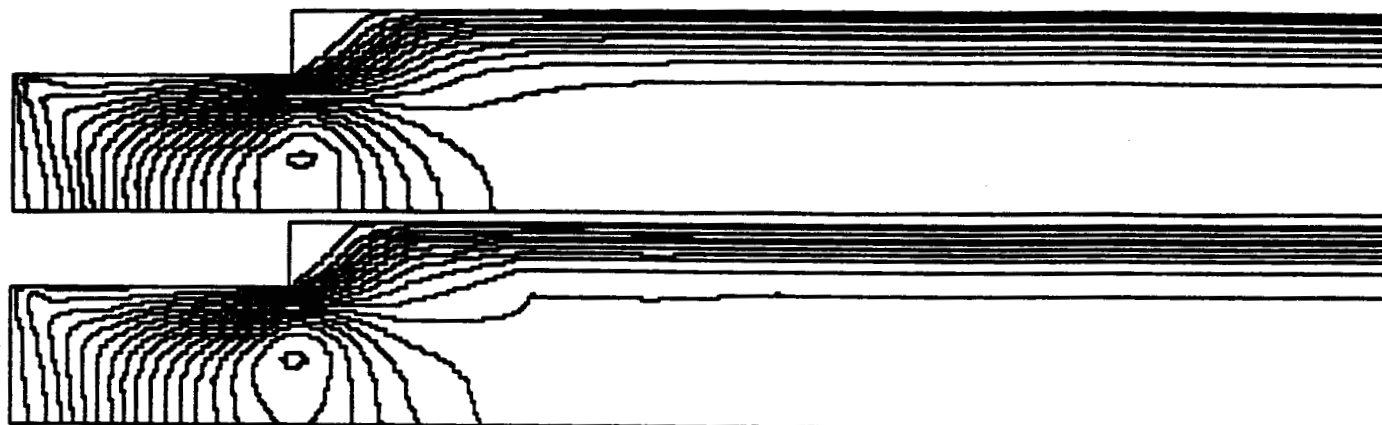


(c)

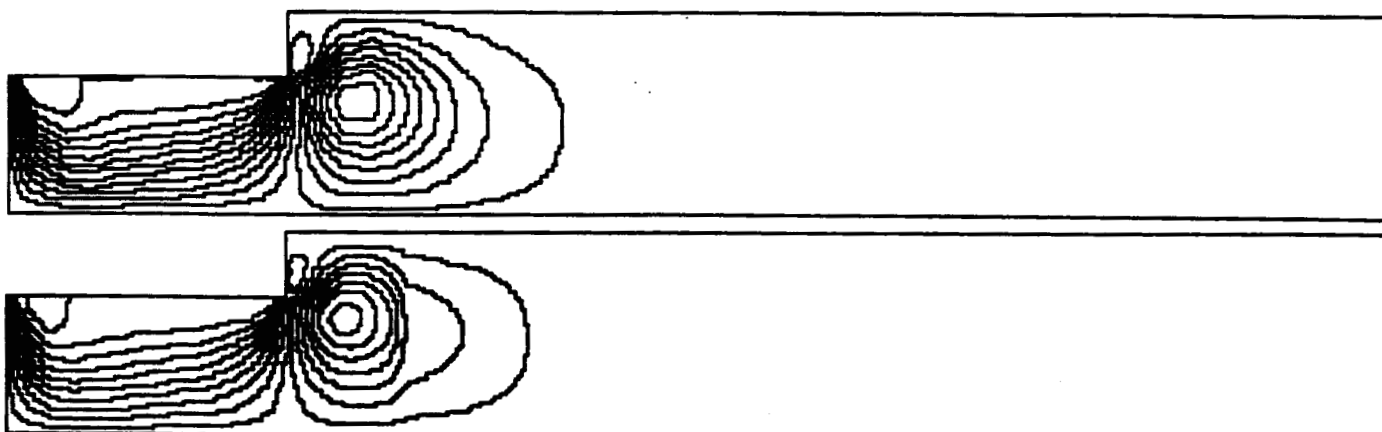
Fif 3. Comparison between the flow field results of the original code (upper part) and those of the revised code (lower part), for (a) the pressure, (b) the U-velocity, and (c) the V-velocity. ($Re=1000.$)



(a)

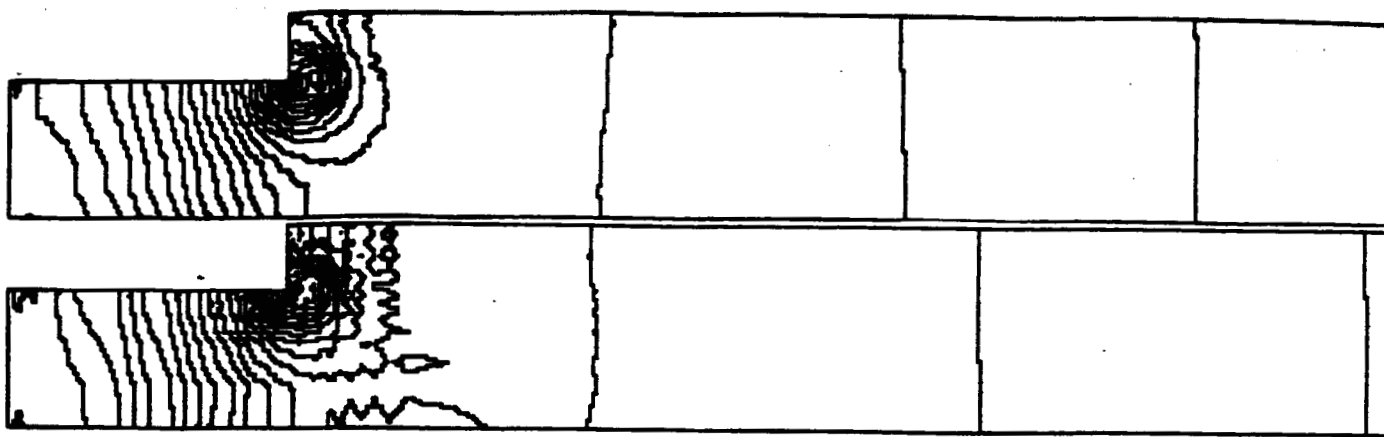


(b)

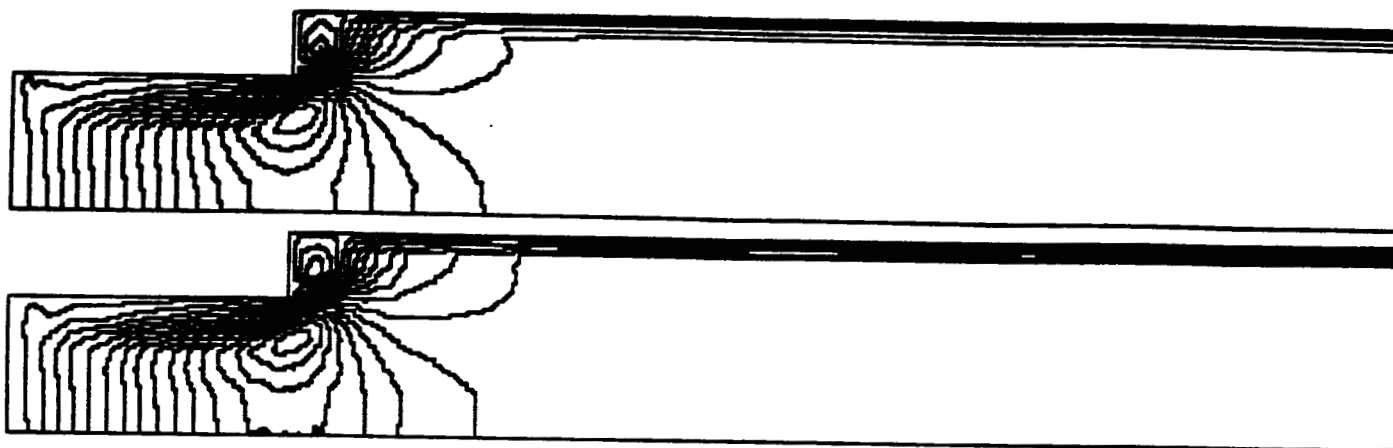


(c)

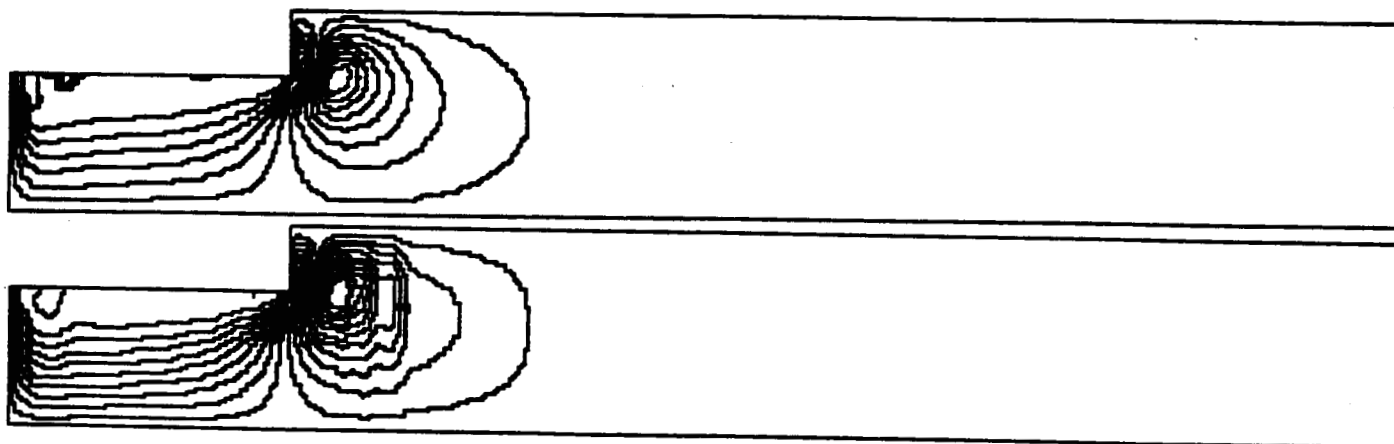
Fig 4. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity; $Re = 1000$.



(a)

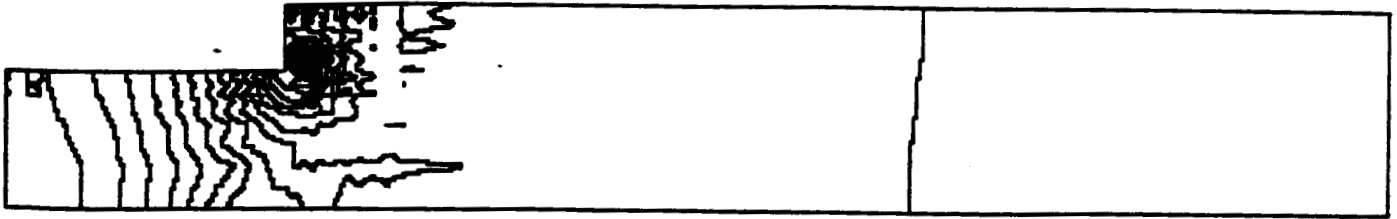
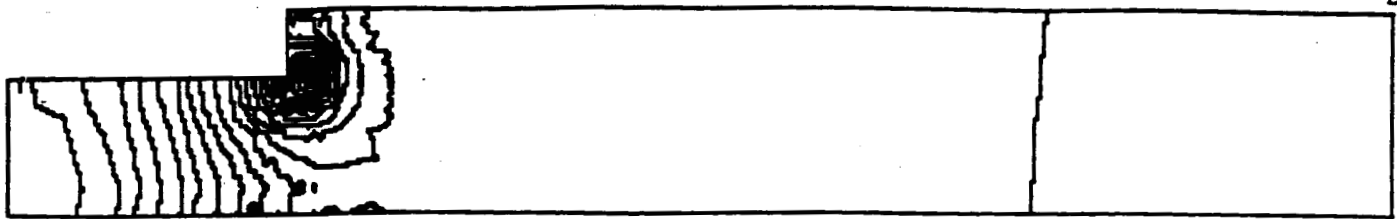


(b)

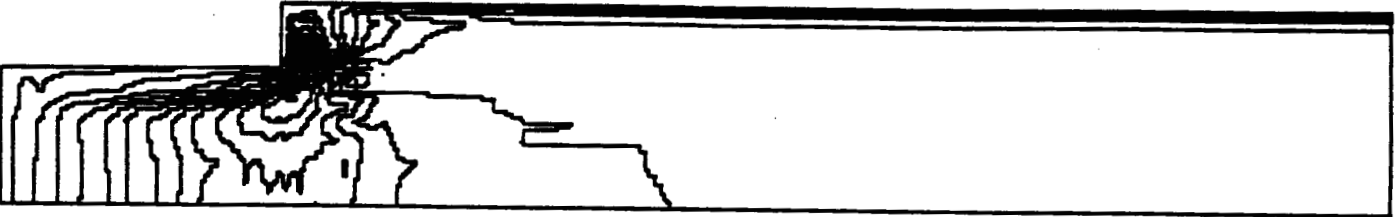
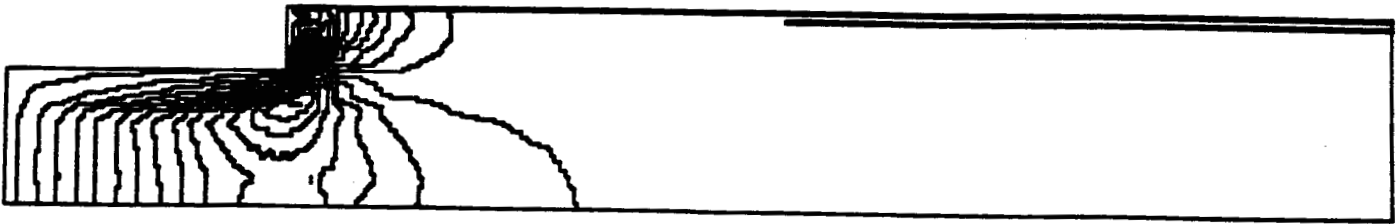


(c)

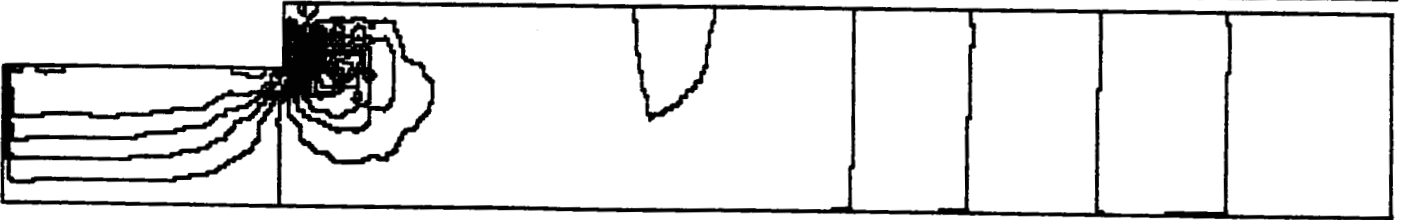
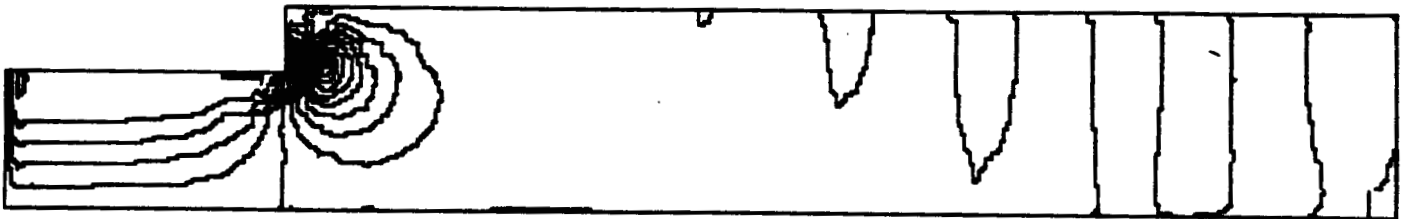
Fig 5. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity; $Re = 10000$.



(a)



(b)



(c)

Fig 6. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity; $Re = 100000$.

Table 1. Comparison between the storage and runtime of the original code and the revised one, at $Re = 10^3$.
(original grids)

	Memory Requirement Bytes	Fraction of the original	Run-time (UNIVAC) min	Fraction of the original	MI (needed)
ORIGINAL	3023004	1	226	1	16
REVISED	3109452	1.02	223	.98	21

Table 2. The reduced grids.

		Parameters	No. of Nodes	No. of Elements
Flow Field	Original	(8,13,17,26)	832	767
	Reduced	(6,9,13,20)	466	417
A/V Field	Original	(2,3,4,3)	40	27
	Reduced	(2,2,2,2)	21	12

Table 3. Storage and run-time comparison between the original grids and the reduced ones. (MI was set at 65 as an initial assumption).

	Re	Memory Requirement Bytes	Fraction of the Original	Run-time (UNIVAC) min	Fraction of the Original	MI (needed)
Original GRID	10^3	3109452	1.	223	1.	21
	10^4	3109452	1.	240	1.	30
	10^5	3109452	1.	242	1.	33
Flow field reduced (only)	10^3	2682808	.86	80	.358	19
	10^4	2682808	.86	100	.420	27
	10^5	2682808	.86	105	.434	33
Flow & A/V fields reduced	10^3	1077816	.34	52	.233	7
	10^4	1077816	.34	64	.267	12
	10^5	1077816	.34	65	.270	14

APPENDIX

Listing of the Revised Code.

MAIN2

ORIGINAL FILE
OF POOR QUALITY

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 01 OF 50

```

1 C
11 C      PROGRAM ISAP1
1 C      VIRTUAL A,A2,B,B2,C,CZ22,D,S,SI,SR
1 C      VIRTUAL PAA,PAH,PAT,UUI,UUR,VVI,VVR
1 C
1 C      PPROGRAM FOR SRB VORTICALLY-COUPLED COMBUSTION INSTABILITY
1 C      ANALYSIS BY FINITE ELEMENTS
1 C
7 C      PARAMETER (NELF1=6,NELF2=9,NETP1=13,NETP2=20)
1 C      PARAMETER (NELF1=8,NELF2=13,NETP1=17,NETP2=26)
1 C      PARAMETER (NALF1=2,NALF2=3,NATP1=4,NATP2=3)
7 C      PARAMETER (NALF1=2,NALF2=2,NATP1=2,NATP2=2)
1 C
7 C      PARAMETER (MI=65,NC1=20,NBP=6,
6 C      &NERGT=NELF1+NELF2,NEBOT=NETP1+NETP2,
6 C      &NEL=NETP2+NERGT+NETP1+NELF2,NBO=2+NERGT+7,
6 C      &NARGT=NALF1+NALF2,NABOT=NATP1+NATP2,
6 C      &NPT1A=(NALF2+1)*NATP1,NPT2A=(NATP2+1)*(NARGT+1),
6 C      &NL=NATP2+NARGT+NATP1+NALF2,NT=NPT1A+NPT2A,MII=4*NT,
6 C      &NT1=NT-NALF1-NALF2-NATP2-2,NTT=3*NT1+NT,
6 C      &NPT1=(NELF2+1)*NETP1,NPT2=(NETP2+1)*(NERGT+1),
6 C      &NGPT=NPT1+NPT2,NBP=NERGT+1,
6 C      &NUX=NELF1+NELF2+NETP1+NETP2+3,NVY=NUX+NBP+NEBOT+1)
1 C
7 C      DIMENSION NENN(NEL,4),NENL(NL,4),ICON(NT),NC(NBP,NC1,2),FRE(NT),
6 C      &PRESS(NT,NT),FVE(MI),UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),
6 C      &VVI(NT,MI)
7 C      DIMENSION NBN1(NELF2+1),NBN2(NELF1+NETP1+1),NBN3(NETP2+1),
6 C      &NBN4(NERG+1),NBN5(NEBOT+1)
1 C
7 C      DIMENSION NODE(NTT),NBQ(NBP),FFNX(NBP),FFNY(NBP),ABN(NBP)
7 C      DIMENSION ANNI(NBP)
7 C      DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11 C      DIMENSION NU(NUX),NV(NVY),ND(NDP),UB(NUX),VB(NVY),PB(NDP)
11 C      DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)
11 C      DIMENSION PFR(NT),PFV(MI),PAA(NT,MI),PAH(NT,MI),PAT(NT,MI)
7 C      DIMENSION US(NGPT),VS(NGPT),DPP(NGPT),DELU(NGPT),DELV(NGPT),
6 C      *A(NGPT,NBO),B(NGPT,NBO),FU(NGPT),FV(NGPT),TARR1(NT),
6 C      *ITER(NT),SR(MII,NTT),SI(MII,NTT),FV1(MII),ITER2(NTT)
7 C      COMPLEX A1(NT,NT),B1(NT,NT),CZ21(NT,NT),EIGAV(NT),EIGBV(NT),
6 C      *EIGV(NT),A2(MII,MII),B2(MII,MII),C(NTT,NTT),D(NTT,NTT),
6 C      *CZ22(NTT,NTT),EIGAV2(NTT),EIGBV2(NTT),EIGV2(NTT)
1 C
7 C      DATA XMIN,XMAX,YMIN,YMAX/O.,10.,O.,1.5/
7 C      DATA XO,YO/2.,1./
1 C
7 C      REN=1000.
7 C      GAMMA=1.2
7 C      DT=1.
7 C      ERROR=.001
7 C      ITMAX=30
7 C      NPT=4
1 C
1 C

```

MAIN2

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT

MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197

DATE: 87/09/24
 TIME: 12:02
 PAGE: 02 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
CT= SPEED OF SOUND(IN/SEC)/CHARACTERISTIC LENGTH(IN)
CT=40000.0/24.0
INPUT DATA
CALL DINPUT(NELF1,NELF2,NETP1,NETP2,NALF1,NALF2,
&NATP2,NERGT,NEBOT,NABOT,NPT1A,NPT1,
&NEL,NGPT,NPT,NBW1,NBW2,NBW3,NBW4,NBW5,NTT,NODE,
&NENN,NENL,ICON,NC,NBN1,NBN2,NBN3,NBN4,NBN5,NT1,NC1,
* XMIN,XMAX,YMIN,YMAX,XO,YO,
* NBQ,XX,YY,UU,VV,PP,NU,NV,ND,UB,VB,PB,FFNX,
* FFFNY,ABN,ANN,REN,GAMMA,DT,ERROR,ITMAX,NL,NT)
COMPUTATION OF MEAN FLOW FIELDS
CALL VELOT(NEL,NGPT,NPT,NBW1,NBW2,XX,YY,UU,VV,PP,REN,DT,ERROR,
* NENN,ICON,XT,YT,UT,VT,NBO,US,VS,DPP,DELU,FU,FV,
* A,B,NUX,NVY,NDP,NU,NV,ND,UB,VB,PB,NT,ITMAX)
COMPUTATION OF ACOUSTIC MODES
CALL EIPRE(NL,NT,NPT,NENL,FRE,PRESS,
* XT,YT,TARR1,A1,B1,CZZ1,EIGAV,EIGBV,EIGV,ITER)
IF(NELF1.GT.1)GOTO 100
COMPUTATION OF VORTICAL MODES
CALL EIVOR(NL,NT,NPT,REN,NTT,NODE,MVP,MT,MII,
* SR,SI,FV1,A2,B2,C,D,CZZ2,EIGAV2,EIGBV2,EIGV2,ITER2,
* NENL,FVE,UUR,UUI,VVR,VVI,XT,YT,UT,VT)
WRITE(6,1000)
DO LOOP FOR EACH ACOUSTIC MODE
DO 1 IK=2,NT
FR=CT*FRE(IK)
PFR(IK)=FR
DO LOOP FOR EACH VORTICAL MODE
DO 1 IG=1,MVP
STABILITY INTEGRAL AT THE BOUNDARY
CALL SURFCE(IK,IG,NBP,FFNX,FFNY,ABN,ANN,NC1,
* NC,FRE,PRESS,FVE,UUR,UUI,VVR,VVI,
* NT,AA,AAB,AHB,AHC,REN,GAMMA,NBQ,MI,
* XT,YT,UT,VT)
STABILITY INTEGRAL IN THE VOLUME

```

ORIGINAL
 OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

PROJECT: CTJJC197 MEMBER: MAIN2 DATE: 87/09/24
GROUP: STB1 LEVEL: 01.00 TIME: 12:02
TYPE: FORT USERID: CTJJC197 PAGE: 03 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8

```
1 C
11 CALL VOLUME(IK,IG,NPT,NL,NT,EN,AAD,AAE,AAF,
6 *
6 *
1 C
1 C
1 C
11 FV2 = FVE(IG)
11 PFV(IG)=FV2
11 CTOEN=CT/EN
9
11 AAA=CTOEN*AAA
11 AAB=CTOEN*AAB
11 AAC=CTOEN*AAC
11 AAD=CTOEN*AAD
11 AAE=CTOEN*AAE
11 AAF=CTOEN*AAF
1 C
11 AHB=CTOEN*AHB
11 AHC=CTOEN*AHC
11 AHE=CTOEN*AHE
11 AHF=CTOEN*AHF
11 AHG=CTOEN*AHG
1 C
11 AA=AAA+AAB+AAC+AAD+AAE+AAF
11 AH=AHB+AHC+AHE+AHF+AHG
11 AT=AA+AH
1 C
11 PAA(IK,IG)=AA
11 PAH(IK,IG)=AH
11 PAT(IK,IG)=AT
1 C
11 WRITE(6,1001) FR,FV2
11 WRITE(6,1002) AT,AA,AH
11 WRITE(6,1012)
11 WRITE(6,1003) AAA,AAB,AAC,AAD,AAE,AAF
11 WRITE(6,1004) AHB,AHC,AHE,AHF,AHG
1 C
11 CONTINUE
1 C
11 WRITE(6,1006)
11 DO 100 IK=1,NT
11 DO 100 IG=1,MVP
11 WRITE(6,1005) PFR(IK),PFV(IG),PAA(IK,IG),PAH(IK,IG),
6 *
11 PAT(IK,IG)
11 CONTINUE
1 100
1 C
1 C
11 STOP
11 FORMAT(////,5X,'STABILITY INTEGRALS',/)
11 FORMAT(//,10X,'ACOUSTIC FREQ =' ,E10.5,'HZ',5X,
6 *
11 'STRAUHAL NO. =' ,E10.5,/)
11 FORMAT(5X,'TOTAL ALP =' ,E15.5,3X,'ACOUSTIC ALP =' ,
6 *
11 E15.5,3X,'VORTICAL ALP =' ,E15.5)
11 FORMAT(20X,'A',14X,'B',14X,'C',14X,'D',14X,'E',
```


MAIN2

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 06 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
DY11=(YMAX-YO)/FLOAT(NELF1)
DO 50 I=1,NETP2+1
K=(I-1)*(NERGT+1)
YY(NPT1+K+1)=YMAX
DO 45 I=1,NELF1-1
YY(NPT1+K+I+1)=YMAX-DY11*FLOAT(I1)
CONTINUE
DO 50 J=1,NELF2+1
YY(NPT1+K+NELF1+J)=YY(J)
CONTINUE
DO 60 I=1,NELF2+1
XX(I)=XMIN
CONTINUE
NO=NELF2+1
DX12=(XO-XMIN)*.5
NTP22=INT(.5*FLOAT(NETP1-1)+.1)
PINV22=1./FLOAT(NTP22)
PINV33=1./FLOAT(NETP1-NTP22)
DO 75 J=2,NETP1
N1=NO
IF(J.EQ.NTP22+1)GOTO 72
IF(J.GT.NTP22)GOTO 73
DUMMY=1.-PINV22*FLOAT(J-1)
DX22=DX12*(1.-ALOG10(10.*DUMMY))
XXOO=XMIN
GOTO 74
XXOO=XMIN
DX22=DX12
GOTO 74
DUMMY=PINV33*FLOAT(J-1-NTP22)
DX22=DX12*ALOG10(10.*DUMMY)
XXOO=XMIN+DX12
DO 75 I=1,NELF2+1
NO=NO+1
XX(N1+I)=XXOO+DX22
CONTINUE
DX33=XO-XMIN
PINV44=1./FLOAT(NETP1+NTP22)
DO 77 J=1,NETP1
N1=NO
DUMMY=1.-PINV44*FLOAT(J-1)
DX34=DX33*(1.-ALOG10(10.*DUMMY))
DO 77 I=1,NERGT+1
NO=NO+1
XX(N1+I)=XO+DX34
CONTINUE
NTP44=NETP2-NETP1
DX44=(XMAX-XX(NO))/FLOAT(NTP44+1)
  
```

ORIGINAL PAGE IS
OF POOR QUALITY

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 07 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11 DO 79 J=1,NTP44+1
11 N1=NO
11 DO 79 I=1,NERGT+1
11 NO=NO+1
11 XX(N1+1)=XX(N1)+DX44
11 CONTINUE
1 79
1 C
11 DO 80 I=1,NGPT
11 PP(I)=O.
11 UU(I)=O.
11 VV(I)=O.
11 CONTINUE
1 80
11 DO 90 I=2,NETP1
11 J=(I-1)*(NELF2+1)
11 VV(J+1)=-O.01
11 CONTINUE
1 90
1 C
11 DO 101 I=1,NELF2+1
11 NBN1(I)=1
11 CONTINUE
1 101
11 DO 102 I=1,NELF1+1
11 NBN2(I)=NPT1+1
11 CONTINUE
1 102
11 DO 103 I=1,NETP1
11 J=I+NELF1+1
11 NBN2(J)=NPT1+1-I*(NELF2+1)
11 CONTINUE
1 103
11 DO 104 I=1,NETP2+1
11 NBN3(I)=NGPT+1-I*(NERGT+1)
11 CONTINUE
1 104
11 DO 105 I=1,NERGT+1
11 NBN4(I)=NGPT-I+1
11 CONTINUE
1 105
11 NN=NELF2+1
11 NBN5(1)=NN
11 DO 106 I=2,NEBOT+1
11 IF(I.GT.NETP1)NN=NERGT+1
11 NBN5(I)=NBN5(I-1)+NN
11 CONTINUE
1 106
1 C
11 N2=O
11 N3=O
11 DO 110 I=1,NELF2+1
11 N2=N2+1
11 N3=N3+1
11 NU(I)=NBN1(I)
11 NV(I)=NBN1(I)
11 CONTINUE
1 110
1 C
11 N4=N2
11 DO 111 I=1,NEBOT+1
11 N2=N2+1
11 NV(N4+1)=NBN5(I)
11 CONTINUE
1 111

```


MAIN2

DATE: 87/09/24
TIME: 12:02
PAGE: 09 OF 50

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

START COL -----1-----2-----3-----4-----5-----6-----7-----+-----8

```

7       NENL(K,2)=J*(NARGT+1)+I+1+NPT1A
7       NENL(K,3)=NENL(K,2)-1
7       NENL(K,4)=NENL(K,1)-1
1 121   CONTINUE
1 C
1 C
7       YDY=(YO-YMIN)/FLOAT(NALF2)
7       ICON(1)=1
7       ICON(NALF2+1)=NELF2+1
7       DO 525 I=2,NALF2
7       YDY1=(NALF2+1-I)*YDY
7       DO 520 J=2,NELF2
7       YINC1=YDY1-VY(J)+YMIN
7       YINC2=YDY1-VY(J+1)+YMIN
7       IF(YINC2.LT.O.)GOTO 520
7       IF(ABS(YINC2).GE.ABS(YINC1))GOTO 521
7       IF(ABS(YINC2).LT.ABS(YINC1))GOTO 522
1 520   CONTINUE
1 521   ICON(I)=J
1       GOTO 525
1 522   ICON(I)=J+1
1 525   CONTINUE
7       IF(NALF2.LE.2)GOTO 526
7       DO 526 I=3,NALF2
7       IF(ICON(I).EQ.ICON(I+1))ICON(I)=ICON(I)-1
7       CONTINUE
1 526
1 C
7       XMID=(XO-XMIN)/2.
7       XDX=(XO-XMIN)/FLOAT(NATP1)
7       DO 535 I=2,NATP1
7       XDX1=(I-1)*XDX
7       DO 530 J=1,NETP1-1
7       JJ1=J*(NELF2+1)+1
7       JJ2=(J+1)*(NELF2+1)+1
7       XINC1=XX(JJ1)-XDX1-XMIN
7       XINC2=XX(JJ2)-XDX1-XMIN
7       IF(XINC2.LT.O.)GOTO 530
7       IF(ABS(XINC2).GE.ABS(XINC1))GOTO 531
7       IF(ABS(XINC2).LT.ABS(XINC1))GOTO 532
1 530   CONTINUE
1 531   JJ=JJ1
1       GOTO 533
1 532   JJ=JJ2
1 533   IF(NATP1.LE.2)GOTO 534
1       LL=-1
1       IF(XX(JJ).GT.XMID)LL=1
1       JK=(I-2)*(NALF2+1)+1
1       IF(ICON(JK).EQ.JJ)JJ=JJ+LL*(NELF2+1)
1 534   ICON((I-1)*(NALF2+1)+1)=JJ
1       DO 535 K=2,NALF2+1
1       KK=(I-1)*(NALF2+1)+K
1       ICON(KK)=ICON(K)+JJ-1
1 535   CONTINUE
1 C

```

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 10 OF 50

MAIN2

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
7      ICON(NPT1A+1)=NPT1+1
7      ICON(NPT1A+NALF1+1)=NPT1+NELF1+1
7      YDY2=(YMAX-YO)/FLOAT(NALF1)
7      DO 545 I=2,NALF1
7      YDY3=(NALF1+1-I)*YDY2
7      DO 540 J=1,NELF1-1
7      YINC3=YDY3-YY(NPT1+J)+YO
7      YINC4=YDY3-YY(NPT1+J+1)+YO
7      IF(YINC4.LT.O.)GOTO 540
7      IF(ABS(YINC4).GE.ABS(YINC3))GOTO 541
7      IF(ABS(YINC4).LT.ABS(YINC3))GOTO 542
1 540  CONTINUE
1 541  ICON(NPT1A+I)=NPT1+J
7      GOTO 545
1 542  ICON(NPT1A+I)=NPT1+J+1
1 545  CONTINUE
7      IF(NALF1.LE.2)GOTO 546
7      DO 546 I=2,NALF1
7      J=NPT1A+I
7      IF(ICON(J).EQ.ICON(J+1))ICON(J)=ICON(J)-1
1 546  CONTINUE
7      DO 547 I=2,NALF2+1
7      ICON(NPT1A+NALF1+I)=NPT1+NELF1+ICON(I)
1 547  CONTINUE
1  C
7      XDX2=(XMAX-XO)/FLOAT(NATP2)
7      DO 555 I=2,NATP2
7      XDX3=(I-1)*XDX2
7      DO 550 J=2,NETP2
7      JJ3=NPT1+J*(NERGT+1)+1
7      JJ4=NPT1+(J+1)*(NERGT+1)+1
7      XINC3=XX(JJ3)-XDX3-XO
7      XINC4=XX(JJ4)-XDX3-XO
7      IF(XINC4.LT.O.)GOTO 550
7      IF(ABS(XINC4).GE.ABS(XINC3))GOTO 551
7      IF(ABS(XINC4).LT.ABS(XINC3))GOTO 552
1 550  CONTINUE
1 551  JJ=JJ3
7      GOTO 553
1 552  JJ=JJ4
1 553  IF(NATP2.LE.2)GOTO 554
7      JK=NPT1A+(I-1)*(NARGT+1)
7      IF(ICON(JK).EQ.JJ)JJ=JJ-(NERGT+1)
1 554  ICON(NPT1A+(I-1)*(NARGT+1)+1)=JJ
7      DO 555 K=2,NARGT+1
7      KK=NPT1A+(I-1)*(NARGT+1)+K
7      ICON(KK)=ICON(NPT1A+K)+JJ-NPT1-1
1 555  CONTINUE
1  C
7      ICON(NT)=NGPT
7      ICON(NT-NARGT)=NGPT-NERGT
7      DO 556 I=2,NARGT
7      J=NT-(NARGT+1)+I
7      JDD=ICON(NPT1A+I)-ICON(NPT1A+I-1)

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 11 OF 50

START COL 1 2 3 4 5 6 7 8

```

7 1 556      ICON(J)=ICON(J-1)+JDD
1 1 C      CONTINUE
1 1 C      :
7 1 1      J1=0
7 1 1      DO 320 J=2,NATP1
7 1 1      DO 320 I=1,NALF2+1
7 1 1      J1=J1+1
7 1 1      NODE(J1)=(J-1)*(NALF2+1)+I
1 1 320      CONTINUE
7 1 1      DO 321 I=1,NALF2
7 1 1      J1=J1+1
7 1 1      NODE(J1)=NPT1A+NALF1+1+I
1 1 321      CONTINUE
7 1 1      DO 322 J=2,NATP2+1
7 1 1      DO 322 I=2,NARGT+1
7 1 1      J1=J1+1
7 1 1      J2=0
7 1 1      IF(I.EQ.2)J2=1
7 1 1      NODE(J1)=NODE(J1-1)+1+J2
1 1 322      CONTINUE
7 1 1      DO 323 I=1,2
7 1 1      DO 323 J=1,NT1
7 1 1      K=I*NT1+J
7 1 1      NODE(K)=NODE(J)+I*NT
1 1 323      CONTINUE
7 1 1      DO 324 I=1,NT
7 1 1      J=3*NT1+I
7 1 1      NODE(J)=NODE(J-1)+1
1 1 324      CONTINUE
1 1 C
1 1 C
7 1 1      DO 350 I=1,6
7 1 1      FFNX(I)=0.
7 1 1      FFNY(I)=0.
7 1 1      ABN(I)=0.
7 1 1      ANN(I)=0.
1 1 350      CONTINUE
7 1 1      NBQ(1)=NALF2
7 1 1      NBQ(2)=NABOT
7 1 1      NBQ(3)=NARGT
7 1 1      NBQ(4)=NATP2
7 1 1      NBQ(5)=NALF1
7 1 1      NBQ(6)=NATP1
7 1 1      DO 360 I=1,6,2
7 1 1      FFNX(I)=1.
7 1 1      FFNY(I+1)=1.
1 1 360      CONTINUE
7 1 1      ABN(6)=1.
7 1 1      ANN(3)=1.
1 1 C
1 1 C
7 1 1      DO 371 J=1,NBQ(1)
7 1 1      NC(1,J,1)=J
  
```

MAIN2

PROJECT: CTJJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 12 OF 50

```

-----1-----2-----3-----4-----5-----6-----7-----8
START COL
7 7 NC(1,J,2)=J+1
1 1 371 CONTINUE
1 C
7 7 K=0
7 7 NBDQ2=NALF2+1
7 7 DO 372 J=1,NBQ(2)
7 7 K=K+NBDQ2
7 7 IF(J.GE.NATP1)NBDQ2=NARGT+1
7 7 NC(2,J,1)=K
7 7 NC(2,J,2)=K+NBDQ2
1 1 372 CONTINUE
1 C
7 7 DO 373 J=1,NBQ(3)
7 7 NC(3,J,1)=NT+1-J
7 7 NC(3,J,2)=NT-J
1 1 373 CONTINUE
1 C
7 7 DO 374 J=1,NBQ(4)
7 7 NC(4,J,1)=NT-J*(NARGT+1)+1
7 7 NC(4,J,2)=NC(4,J,1)-(NARGT+1)
1 1 374 CONTINUE
1 C
7 7 DO 375 J=1,NBQ(5)
7 7 NC(5,J,1)=NPT1A+J
7 7 NC(5,J,2)=NPT1A+J+1
1 1 375 CONTINUE
1 C
7 7 DO 376 J=1,NBQ(6)
7 7 NBDQ6=0
7 7 IF(J.EQ.1)NBDQ6=NALF1
7 7 NC(6,J,1)=NPT1A+1-(J-1)*(NALF2+1)+NBDQ6
7 7 NC(6,J,2)=NPT1A+1-J*(NALF2+1)
1 1 376 CONTINUE
1 C
1 C PRINT INPUT DATA
1 1 WRITE(6,2000)
1 1 WRITE(6,2001) REN,GAMMA
1 1 WRITE(6,2002) DT,ERROR,ITMAX
1 1 WRITE(6,2003) NEL,NGPT,NPT,NBW,NBW1,NBWT
1 C
1 1 WRITE(6,2004)
1 1 DO 1 I=1,NEL
1 1 WRITE(6,1003) (NENN(I,J),J=1,NPT)
1 1 CONTINUE
1 C
1 1 WRITE(6,2005)
1 1 WRITE(6,2006)
1 1 DO 11 I=1,NGPT
1 1 WRITE(6,1004) I,XX(I),YY(I),UU(I),VV(I),PP(I)
1 1 CONTINUE
1 11
1 C
1 1 WRITE(6,2007)
1 1 DO 12 I=1,NUX
1 1 WRITE(6,1005) NU(I),UB(I)

```

MAIN2

MAIN2

PROJECT: CTJC197
 GROUP: S181
 TYPE: FORT

MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197

DATE: 87/09/24
 TIME: 12:02
 PAGE: 13 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
1 12 CONTINUE
11 WRITE(6,2008)
11 DO 13 I=1,NVY
11 WRITE(6,1005) NV(I),VB(I)
1 13 CONTINUE
11 WRITE(6,2009)
11 DO 14 I=1,NDP
11 WRITE(6,1005) ND(I),PB(I)
1 14 CONTINUE
1 C
11 WRITE(6,2010)
11 DO 15 I=1,NTT
11 WRITE(6,1006) I,NODE(I)
1 15 CONTINUE
1 C
11 WRITE(6,2011)
11 WRITE(6,2012)
11 DO 16 I=1,NBP
11 WRITE(6,1007) I,NBQ(I),FFNX(I),FFNY(I),ABN(I),ANN(I)
1 16 CONTINUE
1 C
11 WRITE(6,2013)
11 DO 17 I=1,NBP
11 NB=NBQ(I)
11 DO 17 J=1,NB
11 WRITE(6,1008) (NC(I,J,K),K=1,2)
1 17 CONTINUE
1 C
11 FORMAT(4I5)
11 FORMAT(15,5F10.5)
11 FORMAT(15,F10.5)
11 FORMAT(2I5)
11 FORMAT(2I5,4F10.5)
11 FORMAT(2I5)
11 RETURN
11 FORMAT(///,10X,'INPUT DATA',///)
11 FORMAT(5X,'REN=',E10.5,5X,'GAMMA=',F10.5)
11 FORMAT(5X,'DT=',F10.5,2X,'ERROR=',F10.5,2X,'ITMAX=',I5)
11 FORMAT(5X,'NEL=',I5,2X,'NGPT=',I5,2X,'NPT=',I5,2X,
11 'NBW=',I5,2X,'NBW1=',I5,2X,'NBWT=',I5)
11 FORMAT(///,10X,'ELEMENT CONNECTIVITY MATRIX',/)
11 FORMAT(///,10X,'COORDINATE VALUE AT EACH GLOBAL NODE',/)
11 FORMAT(1X,'NO',7X,'XX',7X,'YY',7X,'UU',7X,'VV',7X,'PP',/)
11 FORMAT(///,10X,'BOUNDARY CONDITIONS FOR MEAN FLOW FIELDS',/)
11 FORMAT(//)
11 FORMAT(//)
11 FORMAT(///,10X,'ADJUSTMENT FOR BOUNDARY CONDITIONS',/)
11 FORMAT(///,10X,'NORMAL VECTORS AND ADMITTANCES',/)
11 FORMAT(1X,'NO',3X,'NEQ',6X,'FFNX',6X,'FFNY',7X,'ABN',
11 7X,'ANN',/)
11 FORMAT(///,10X,'BOUNDARY ELEMENT CONNECTIVITY MATRIX',/)
11 END
1 1 C
1 1 C

```

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 14 OF 50

1-----2-----3-----4-----5-----6-----7-----8
 START COL

```

11 C
11 SUBROUTINE VELOT(NEL,NGPT,NPT,NBW1,NBW2,XX,YY,
6 * UU,VV,PP,REN,DT,ERROR,
6 * NENN,ICON,XT,YT,UT,VT,NBO,US,VS,DPP,DELU,DELV,FU,FV,
6 * A,B,NUX,NVY,NDP,NU,NV,NO,UB,VB,PB,NT,ITMAX)
1 C
1 C VIRTUAL
1 C
1 C SUBROUTINE FOR MEAN VELOCITY CALCULATIONS
1 C
1 C A(NGPT,NBWT) : GLOBAL BAND STIFFNESS MATRIX
1 C B(NGPT,NBWT) : GLOBAL BAND STIFFNESS MATRIX
1 C FN(NGPT) : GLOBAL FORCE MATRIX
1 C FV(NGPT) : GLOBAL FORCE MATRIX
1 C US(NGPT) : ESTIMATED U-VELOCITY
1 C VS(NGPT) : ESTIMATED V-VELOCITY
1 C DPP(NGPT) : PRESSURE CORRECTIONS
1 C DELU(NGPT) : ACCELERATIONS IN X-DIRECTION
1 C DELV(NGPT) : ACCELERATIONS IN Y-DIRECTION
1 C ST(4) : GAUSSIAN POINTS OF GAUSSIAN QUADRATURE
1 C WS(4) : WEIGHTING FUNCTIONS OF GAUSSIAN QUADRATURE
1 C ANM(NPT,NPT) : LOCAL STIFFNESS MATRIX
1 C BNM(NPT,NPT) : LOCAL STIFFNESS MATRIX
1 C CNM(NPT,NPT) : LOCAL STIFFNESS MATRIX
1 C FNU(NPT) : LOCAL FORCE MATRIX
1 C FNV(NPT) : LOCAL FORCE MATRIX
1 C GN(NPT) : LOCAL FORCE MATRIX
1 C HNU(NPT) : LOCAL FORCE MATRIX
1 C HNV(NPT) : LOCAL FORCE MATRIX
1 C SUM : CONVERGENCE ERROR IN EACH ITERATION
1 C ITER : COUNTER OF ITERATION
1 C
11 DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)
11 DIMENSION UB(NUX),VB(NVY),PB(NDP),WS(4),ST(4)
11 DIMENSION NU(NUX),NV(NVY),ND(NDP)
7 DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11 DIMENSION US(NGPT),VS(NGPT),DPP(NGPT),DELU(NGPT),DELV(NGPT)
11 DIMENSION ANM(4,4),BNM(4,4),CNM(4,4),FNU(4),FNV(4),GN(4),
6 HNU(4),HNV(4),A(NGPT,NBO),B(NGPT,NBO),
6 FU(NGPT),FV(NGPT),NENN(NEL,4),ICON(NT)
1 C
1 C CALL THE VALUES FOR GAUSSIAN QUADRATURE INTEGRATIONS
1 C
1 C CALL GAUSS(4,WS,ST)
1 C
1 C ITER=0
1 C
1 C CONTINUE
1 C
1 C ITER=ITER+1
1 C
1 C ESTIMATED VELOCITIES
1 C
1 C DO 100 I=1,NGPT
11

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 15 OF 50

MAIN2

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      FU(I)=0.0
11      FV(I)=0.0
11      DO 100 J=1,NBWT
11      A(I,J)=0.0
11      B(I,J)=0.0
11      CONTINUE
11      100
11      C
11      DO 200 I=1,NEL
11      CALL ELEUV(I,NPT,NGPT,XX,YY,UU,VV,PP,REN,DT,NENN,
11      *      ANM,FNU,FNV,WS,ST,NEL)
11      DO 200 J=1,NPT
11      JJ=NENN(I,J)
11      FU(JJ)=FU(JJ)+FNU(J)
11      FV(JJ)=FV(JJ)+FNV(J)
11      DO 200 K=1,NPT
11      KK=NENN(I,K)
11      KKJJ=KK-JJ+NBW1
11      A(JJ,KKJJ)=A(JJ,KKJJ)+ANM(J,K)
11      B(JJ,KKJJ)=A(JJ,KKJJ)
11      CONTINUE
11      200
11      C
11      CALL ADJUST(NUX,NGPT,NU,A,UB,FU,NBW1,NBWT)
11      CALL ADJUST(NVY,NGPT,NV,B,VB,FV,NBW1,NBWT)
11      C
11      CALL GAUSU(A,FU,US,NGPT,NBW1,NBWT)
11      CALL GAUSU(B,FV,VS,NGPT,NBW1,NBWT)
11      C
11      C
11      PRESSURE CORRECTIONS
11      DO 300 I=1,NGPT
11      FU(I)=0.0
11      DO 300 J=1,NBWT
11      A(I,J)=0.0
11      CONTINUE
11      300
11      C
11      DO 400 I=1,NEL
11      CALL ELEPR(I,NPT,NGPT,XX,YY,US,VS,DT,BNM,GN,
11      *      WS,ST,NEL,NENN)
11      DO 400 J=1,NPT
11      JJ=NENN(I,J)
11      FU(JJ)=FU(JJ)+GN(J)
11      DO 400 K=1,NPT
11      KK=NENN(I,K)
11      KKJJ=KK-JJ+NBW1
11      A(JJ,KKJJ)=A(JJ,KKJJ)+BNM(J,K)
11      CONTINUE
11      400
11      C
11      CALL ADJUST(NDP,NGPT,ND,A,PB,FU,NBW1,NBWT)
11      CALL GAUSU(A,FU,DPP,NGPT,NBW1,NBWT)
11      C
11      ACCELERATIONS
11      DO 500 I=1,NGPT
11

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 16 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      FU(I)=0.0
11      FV(I)=0.0
11      DO 500 J=1,NBWT
11      A(I,J)=0.0
11      B(I,J)=0.0
11      CONTINUE
11      500 C
11
11      DO 600 I=1,NEL
11      CALL ELEAC(I,NPT,NGPT,XX,YY,DPP,CNM,HNU,HNV,
11      WS,ST,NEL,NENN)
11      600
11      DO 600 J=1,NPT
11      JJ=NENN(I,J)
11      FU(JJ)=FU(JJ)+HNU(J)
11      FV(JJ)=FV(JJ)+HNV(J)
11      DO 600 K=1,NPT
11      KK=NENN(I,K)
11      KKJJ=KK-JJ+NBW1
11      A(JJ,KKJJ)=A(JJ,KKJJ)+CNM(J,K)
11      B(JJ,KKJJ)=A(JJ,KKJJ)
11      CONTINUE
11      600 C
11
11      CALL GAUSU(A,FU,DELU,NGPT,NBW1,NBWT)
11      CALL GAUSU(B,FV,DELV,NGPT,NBW1,NBWT)
11
11      CORRECTIONS OF PRESSURE AND VELOCITIES
11
11      DO 700 I=1,NGPT
11      PP(I)=PP(I)+DPP(I)
11      UU(I)=US(I)+DELU(I)*DT
11      VV(I)=VS(I)+DELV(I)*DT
11      CONTINUE
11      700 C
11
11      CALCULATIONS OF CONVERGENCE ERROR
11
11      SUM1=0.0
11      SUM2=0.0
11      DO 800 I=1,NGPT
11      SUM1=SUM1+(DELU(I)*DT)**2
11      SUM2=SUM2+UU(I)**2
11      CONTINUE
11      SUM=SQRT(SUM1/SUM2)
11      800 C
11
11      IF(ITER.GT.ITMAX) GO TO 3000
11      IF(SUM.GT.ERROR) GO TO 2000
11
11      CONTINUE
11      3000 C
11
11      DO 900 I=1,NGPT
11      UU(I)=US(I)
11      VV(I)=VS(I)
11      CONTINUE
11      900 C
11
11      DO 910 I=1,NT
11      K=ICON(I)
11

```

-MAIN2

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT

MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197

DATE: 87/09/24
 TIME: 12:02
 PAGE: 17 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      XT(I)=XX(K)
11      YT(I)=YY(K)
11      UT(I)=UU(K)
11      VT(I)=VV(K)
11      CONTINUE
11      910
11      1 C
11      1 C
11      1 C
11      OUTPUT FOR CONVERGED MEAN VELOCITY FIELDS
11      WRITE(6,5000) ITER,SUM
11      WRITE(6,5010)
11      DO 1200 I=1,NGPT
11      WRITE(6,5020) I, XX(I),YY(I),UU(I),VV(I),PP(I)
11      CONTINUE
11      1200
11      1 C
11      RETURN
11      FORMAT(//////,10X,'ITER=',2X,I5,5X,'ERROR=',2X,E15.8,/)
11      FORMAT(8X,'NO',4X,'XX',8X,'YY',14X,'UU',13X,'VV',
11      13X,'PP',)
11      6
11      5020
11      FORMAT(5X,I5,2F10.5,3E15.5)
11      END
11      1 C
11      1 C
11      SUBROUTINE EIPRE(NL,NT,NPT,NENL,FRE,PRESS,
11      * XT,YT,TARR1,A1,B1,CZ1,EIGAV,EIGBV,EIGV,ITER)
11      VIRTUAL
11      SUBROUTINE FOR ACOUSTIC MODES
11      FRE(NGPT) : ACOUSTIC FREQUENCIES
11      PRESS(NGPT,NGPT) : ACOUSTIC MODES
11      A1(NGPT,NGPT) : LEFT-HAND-SIDE GLOBAL EIGENMATRIX
11      B1(NGPT,NGPT) : RIGHT-HAND-SIDE GLOBAL EIGENMATRIX
11      CZ1(NGPT,NGPT) : SOLUTIONS OF EIGENVECTORS
11      EIGAV(NGPT) : SOLUTIONS OF EIGENVECTORS
11      EIGBV(NGPT) : SOLUTIONS OF EIGENVECTORS
11      EIGV(NGPT) : EIGAV(NGPT)/EIGBV(NGPT)
11      ANM(NPT,NPT) : LEFT-HAND-SIDE LOCAL EIGENMATRIX
11      BNM(NPT,NPT) : RIGHT-HAND-SIDE LOCAL EIGENMATRIX
11      1 C
11      7
11      DIMENSION XT(NT),YT(NT)
11      DIMENSION TARR1(NT),WS(4),ST(4),ANM(4,4),BNM(4,4)
11      *, NENL(NL,4),FRE(NT),PRESS(NT,NT)
11      6
11      COMPLEX A1(NT,NT),B1(NT,NT),CZ1(NT,NT),EIGAV(NT),
11      * EIGBV(NT),EIGV(NT)
11      6
11      INTEGER ITER(NT)
11      1 C
11      CALL GAUSS(4,WS,ST)
11      1 C
11      1 C
11      1 C
11      INITIALIZATION OF ALL GLOBAL MATRICES
11      1 C
11      DO 190 I=1,NT
11      DO 190 J=1,NT
11      A1(I,J)=(0.0,0.0)
11      B1(I,J)=(0.0,0.0)

```

DATE: 87/09/24
TIME: 12:02
PAGE: 18 OF 50

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

```

START COL 1 190 CONTINUE
1 C
1 C ASSEMBLY OF GLOBAL MATRICES
1 C
11 DO 200 I=1,NL
11 CALL ELEMPT(I,NPT,ANM,BNM,WS,ST,NL,NT,NENL,
6 * XT,YT)
1 C
11 DO 200 J=1,NPT
11 JJ=NENL(I,J)
11 DO 200 K=1,NPT
11 KK=NENL(I,K)
11 A1(JJ,KK)=A1(JJ,KK)+CMPLX(ANM(J,K),O.O)
11 B1(JJ,KK)=B1(JJ,KK)+CMPLX(BNM(J,K),O.O)
11 CONTINUE
1 200
1 C
1 C APPLY EIGENVALUE SUBROUTINE IN IMSL
1 C
11 CALL CONVRT(NT,A1,NT,B1,NT,CZZ1,NT)
11 CALL SOLVE(NT,A1,NT,B1,NT,CZZ1,NT,ITER,EIGAV,EIGBV)
1 C
1 C OBTAIN EIGENVALUES AND EIGENVECTORS
1 C
11 DO 220 IEG=1,NT
11 IF(EIGBV(IEG).EQ.O.O) GO TO 220
11 EIGV(IEG)=EIGAV(IEG)/EIGBV(IEG)
11 FRE(IEG)=SORT(ABS(REAL(EIGV(IEG))))
11 DO 221 IEF=1,NT
11 PRESS(IEF,IEG)=REAL(CZZ1(IEF,IEG))
11 CONTINUE
1 221
1 220 CONTINUE
1 C
1 C SORTING PROCESS
1 C
11 NN=NT-1
11 DO 4000 K=1,NN
11 JJ=NT-K
11 DO 410 L=1,JJ
11 IF(FRE(L).LE.FRE(L+1)) GO TO 410
11 TEMP=FRE(L)
11 FRE(L)=FRE(L+1)
11 FRE(L+1)=TEMP
11 DO 420 NP=1,NT
11 TARR1(NP)=PRESS(NP,L)
11 PRESS(NP,L)=PRESS(NP,L+1)
11 PRESS(NP,L+1)=TARR1(NP)
11 CONTINUE
1 420
1 410 CONTINUE
1 4000 CONTINUE
1 C
1 C OUTPUT FOR ACOUSTIC FREQUENCIES AND THEIR MODES
11 WRITE(6,1000)
11 DO 500 I=1,NT

```

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 19 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      WRITE(6,1001) I,FRE(I)
11      CONTINUE
11      WRITE(6,1002)
11      DO 501 I=1,NT
11      WRITE(6,1003) I-1,FRE(I)
11      WRITE(6,1013)
11      DO 502 J=1,NT
11      WRITE(6,1004) J,XT(J),YT(J),PRESS(J,I)
11      CONTINUE
11      WRITE(6,1005)
11      CONTINUE
11      RETURN
11      FORMAT(//,10X,'ACOUSTIC FREQUENCIES',/)
11      FORMAT(15X,15,E15.5)
11      FORMAT(//,10X,'LOWEST TWENTY ACOUSTIC MODES',/)
11      FORMAT(10X,15,'-TH ACOUSTIC MODE',5X,'FRE = ',E15.5)
11      FORMAT(8X,'NO',4X,'XX',8X,'YY',14X,'PRESS')
11      FORMAT(5X,15,2F10.5,E15.5)
11      FORMAT(//)
11      END
11      C
11      C
11      C
11      C
11      SUBROUTINE EIVOR(NL,NT,NPT,REN,NTT,NODE,MVP,MI,MII,'
* SR,SI,FV1,A2,B2,C,D,CZ2,EIGAV2,EIGBV2,EIGV2,ITER2,
* NENL,FVE,UUR,UUI,VVR,VVI,XT,YT,UT,VT)
11      VIRTUAL
11      C
11      C
11      C
11      C
11      SUBROUTINE FOR VORTICAL MODES
11      C
11      MVP      : NUMBER OF USEFUL VORTICAL EIGENMODES
11      FVE(MVP) : VORTICAL FREQUENCIES
11      UUR(NT,MVP) : REAL PART OF VORTICAL DISTURBANCES OF
11                  U-VELOCITY
11      VVR(NT,MVP) : REAL PART OF VORTICAL DISTURBANCES OF
11                  V-VELOCITY
11      UUI(NT,MVP) : IMAGINARY PART OF VORTICAL DISTURBANCES OF
11                  U-VELOCITY
11      VVI(NT,MVP) : IMAGINARY PART OF VORTICAL DISTURBANCES OF
11                  V-VELOCITY
11      C(NTT,NTT) : LEFT-HAND-SIDE GLOBAL EIGENMATRIX
11      D(NTT,NTT) : RIGHT-HAND-SIDE GLOBAL EIGENMATRIX
11      CZ2(NTT,NTT) : SOLUTIONS OF EIGENVECTORS
11      EIGAV2(NTT) : SOLUTIONS OF EIGENVALUES
11      EIGBV2(NTT) : SOLUTIONS OF EIGENVALUES
11      EIGV2(NTT) : EIGAV2(NTT)/EIGBV2(NTT)
11      SR(4*NT,4*NT) : REAL PART OF CZ2(NTT,NTT)
11      SI(4*NT,4*NT) : IMAGINARY PART OF CZ2(NTT,NTT)
11      ANM(4,4,4,4) : LEFT-HAND-SIDE OF LOCAL EIGENMATRIX
11      BNM(4,4,4,4) : RIGHT-HAND-SIDE OF LOCAL EIGENMATRIX
11      C
11      C
11      C
11      C
11      DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11      DIMENSION SR(MII,NTT),SI(MII,NTT),NODE(NTT)

```


PROJECT: CTJJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 22 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11 WRITE(6,999)
11 DO 10 I=1,20
11 WRITE(6,1000) I,FVE(I)
11 WRITE(6,1010)
11 DO 11 J=1,NF
11 WRITE(6,1001) J,XT(J),YT(J),UUR(J,I),UUI(J,I),
        * VVR(J,I),VVI(J,I)
11 CONTINUE
11 CONTINUE
11 RETURN
11 FORMAT(//////,10X,'LOWEST TWENTY VORTICAL MODES',/)
11 FORMAT(//////,15,'-TH VORTICAL MODE',5X,
        * 'STROUHAL NO. =',E10.5,/)
11 FORMAT(3X,'NO',5X,'XT',8X,'YT',9X,'UUR',12X,'UUI',
        * 12X,'VVR',12X,'VVI')
11 FORMAT(15,2F9.5,4E14.5)
11 END

```

```

SUBROUTINE SURFCE(IK,IG,NBP,FFNX,FFNY,ABN,ANN,NC1,
        * NC,FRE,PRESS,FVE,UUR,UUI,VVR,VVI,
        * NT,AAA,AAB,
        * AHB,AHC,REN,GAMMA,NBQ,MI,
        * XT,YT,UT,VT)

```

VIRTUAL

STABILITY INTEGRALS AT THE SURFACES

```

IK : COUNTER OF ACOUSTIC MODES
IG : COUNTER OF VIRTICAL MODES
AAA : (A)-TERM OF ACOUSTIC GROWTH CONSTANT
AAB : (B)-TERM OF ACOUSTIC GROWTH CONSTANT
AHB : (B)-TERM OF VORTICALLY COUPLED ACOUSTIC
        * GROWTH CONSTANT
AHC : (C)-TERM OF VORTICALLY COUPLED ACOUSTIC
        * GROWTH CONSTANT
X(2) : LOCAL BOUNDARY X-COORDINATES
Y(2) : LOCAL BOUNDARY Y-COORDINATES
U(2) : LOCAL BOUNDARY MEAN VELOCITY IN X-DIRECTION
V(2) : LOCAL BOUNDARY MEAN VELOCITY IN Y-DIRECTION
P(2) : LOCAL BOUNDARY ACOUSTIC MODES
UR(2) : LOCAL BOUNDARY VALUE OF REAL PART OF VORTICAL
        * DISTURBANCES IN X-DIRECTION
VR(2) : LOCAL BOUNDARY VALUE OF REAL PART OF VORTICAL
        * DISTURBANCES IN Y-DIRECTION
UI(2) : LOCAL BOUNDARY VALUE OF IMAGINARY PART OF
        * VORTICAL DISTURBANCES IN X-DIRECTION
VI(2) : LOCAL BOUNDARY VALUE OF IMAGINARY PART OF
        * VORTICAL DISTURBANCES IN Y-DIRECTION
FI(2) : INTERPOLATION FUNCTIONS IN BOUNDARY ELEMENT
DS(2) : FIRST DERIVATIVES OF INTERPOLATION FUNCTIONS

```

```

PROJECT: CTJJC197      MEMBER: MAIN2      DATE: 87/09/24
GROUP:   STB1         LEVEL:  01.00      TIME: 12:02
TYPE:    FORT         USERID: CTJJC197   PAGE: 23 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8
1 C      IN BOUNDARY ELEMENT
1 C
7
11 DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11 DIMENSION FFNX(NBP),FFNY(NBP),ABN(NBP),ANN(NBP),NBQ(NBP)
11 DIMENSION U(2),V(2),
6 * WS(4),ST(4),X(2),Y(2),P(2),UI(2),VI(2),FI(2),DS(2)
11 DIMENSION UR(2),VR(2),NC(NBP,NC1,2),FRE(NT),PRESS(NT,NT),
6 * FVE(MI),UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),VVI(NT,MI)
1 C CALL GAUSS(4,WS,ST)
11
1 C FR=FRE(IK)
11 FRINV=1./FR
7 FR2INV=FRINV*FRINV
7 RFRINV=FRINV/REN
11 FV3=FVE(IG)
1 C
1 C INITIALIZATIONS
1 C
11 AAA=O.O
11 AAB=O.O
11 AHB=O.O
11 AHC=O.O
1 C
1 C REPEAT INTEGRATION IN EACH BOUNDARY AREA
1 C
11 DO 1 IB=1,NBP
1 C IF(IB.EQ.2) GO TO 1
1 C
1 C NECESSARY INFORMATION IN EACH BOUNDARY AREA
1 C
11 FNX=FFNX(IB)
11 FNY=FFNY(IB)
11 NB = NBQ(IB)
11 AB = ABN(IB)
11 AN = ANN(IB)
1 C
11 DO 2 IC=1,NB
1 C
11 DO 10 N=1,2
11 NN=NC(IB,IC,N)
11 X(N)=XT(NN)
11 Y(N)=YT(NN)
11 U(N)=UT(NN)
11 V(N)=VT(NN)
11 P(N)=PRESS(NN,IK)
11 UR(N)=UUR(NN,IG)
11 VR(N)=VVR(NN,IG)
11 UI(N)=UUI(NN,IG)
11 VI(N)=VVI(NN,IG)
11 CONTINUE
1 C
11 IF(FNX .EQ. O.O) DTA=O.5*ABS(X(2))-X(1))
11

```

MAIN2

PROJECT: CTJJC197
 GROUP: STB1
 TYPE: FORT

MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJJC197

DATE: 87/09/24
 TIME: 12:02
 PAGE: 24 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      IF(FNY .EQ. 0.0) DTA=0.5*ABS(Y(2)-Y(1))
7      DTINV5=-.5/DTA
1      C
11      DO 100 K=1,4
11      XI=ST(K)
11      ACOF=WS(K)
1      C
11      INTERPOLATION FUNCTIONS AT THE BOUNDARY ELEMENT
1      C
11      FI(1)=0.5*(1.0-XI)
11      FI(2)=0.5*(1.0+XI)
1      C
11      DS(1)=DTINV5
11      DS(2)=-DS(1)
1      C
11      YP=0.0
11      SU=0.0
11      SV=0.0
11      PN=0.0
11      PS=0.0
11      SUI=0.0
11      SUI5=0.0
11      SVIS=0.0
1      C
11      DO 110 N=1,2
11      YP=YP+FI(N)*Y(N)
11      SU=SU+FI(N)*U(N)
11      SV=SV+FI(N)*V(N)
11      PN=PN+FI(N)*P(N)
11      PS=PS+DS(N)*P(N)
11      SUI=SUI+FI(N)*UI(N)
11      SVI=SVI+FI(N)*VI(N)
11      SUI5=SUI5+DS(N)*UI(N)
11      SVIS=SVIS+DS(N)*VI(N)
11      CONTINUE
1      110
1      C
11      C=3.14159*YP*ACOF*DTA
1      C
11      AAA=AAA+C*((AB-AN)*PN*PN+(GAMMA+1.0)*(SU*FNX+SV*FNY)*PN*PN)
11      AAB=AAB-C*(SU*FNX+SV*FNY)*PS*PS*FR2INV
11      AHB=AHB+C*GAMMA*(2.0*(SU*SUI*PS*FNX+SV*SVI*PS*FNY)
6      *      +(SU*SVI+SV*SUI)*PS*(FNX*FNY))*FRINV
11      AHC=AHC+C*(SVIS*PS*FNX+SUI5*PS*FNY)*RFRINV
11      CONTINUE
1      100
1      C
11      CONTINUE
1      2
1      1
1      1
1      C
11      RETURN
11      END
1      C
1      C
1      C
11
SUBROUTINE VOLUME(IK,IG,NPT,NL,NT,EN,AAD,AAE,AAF,

```

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

*      *
*      *      NENL,FRE,PRESS,UUR,UUI,VVR,VVI,
*      *      AHE,AHF,AHG,REN,GAMMA,MI,XT,YT,UT,VT)
*      *
*      *      VIRTUAL
*      *
*      *      STABILITY INTEGRALS IN THE VOLUME
*      *
*      *      IK      : COUNTER OF ACOUSTIC MODES
*      *      IG      : COUNTER OF VORTICAL MODES
*      *      EN      : DENOMINATOR OF EACH STABILITY INTEGRAL TERM
*      *      AAD      : (D)-TERM OF ACOUSTIC GROWTH CONSTANT
*      *      AAE      : (E)-TERM OF ACOUSTIC GROWTH CONSTANT
*      *      AAF      : (F)-TERM OF ACOUSTIC GROWTH CONSTANT
*      *      AHE      : (E)-TERM OF VORTICALLY COUPLED ACOUSTIC
*      *      : GROWTH CONSTANT
*      *      AHF      : (F)-TERM OF VORTICALLY COUPLED ACOUSTIC
*      *      : GROWTH CONSTANT
*      *      AHG      : (G)-TERM OF VORTICALLY COUPLED ACOUSTIC
*      *      : GROWTH CONSTANT
*      *      X(NPT)   : LOCAL X-COORDINATES
*      *      Y(NPT)   : LOCAL Y-COORDINATES
*      *      U(NPT)   : LOCAL VALUES OF MEAN VELOCITIES IN
*      *      : X-DIRECTION
*      *      V(NPT)   : LOCAL VALUES OF MEAN VELOCITIES IN
*      *      : Y-DIRECTION
*      *      P(NPT)   : LOCAL VALUES OF ACOUSTIC MODES
*      *      UR(NPT)   : LOCAL VALUES OF REAL PART OF VORTICAL
*      *      : DISTURBANCES IN X-DIRECTION
*      *      VR(NPT)   : LOCAL VALUES OF REAL PART OF VORTICAL
*      *      : DISTURBANCES IN Y-DIRECTION
*      *      UI(NPT)   : LOCAL VALUES OF IMAGINARY PART OF
*      *      : VORTICAL DISTURBANCES IN X-DIRECTION
*      *      VI(NPT)   : LOCAL VALUES OF IMAGINARY PART OF
*      *      : VORTICAL DISTURBANCES IN Y-DIRECTION
*      *      FI(NPT)   : INTERPOLATION FUNCTIONS
*      *      DX(NPT)   : FIRST DERIVATIVES OF INTERPOLATION
*      *      : FUNCTIONS IN X-DIRECTION
*      *      DY(NPT)   : FIRST DERIVATIVES OF INTERPOLATION
*      *      : FUNCTIONS IN Y-DIRECTION
*      *      DXX(NPT)  : SECOND DERIVATIVES OF INTERPOLATION
*      *      : FUNCTIONS IN X-DIRECTION
*      *      DXY(NPT)  : SECOND DERIVATIVES OF INTERPOLATION
*      *      : FUNCTIONS IN X- AND Y-DIRECTION
*      *      DYY(NPT)  : SECOND DERIVATIVES OF INTERPOLATION
*      *      : FUNCTIONS IN Y-DIRECTION
*      *
*      *      DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
*      *      : DIMENSION X(4),Y(4),U(4),V(4),P(4),UR(4),VR(4),UI(4),VI(4),
*      *      : FI(4),DX(4),DY(4),AA(4),AB(4),DXX(4),DXY(4),
*      *      : DYY(4),WS(4),ST(4),NENL(NL,4),FRE(NT),PRESS(NT,NT),
*      *      : UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),VVI(NT,MI)
*      *
*      *      CALL GAUSS(4,WS,ST)
*      *      FR=FRE(IK)

```

```

PROJECT: CTJJC197      MEMBER: MAIN2      DATE: 87/09/24
GROUP:   STB1          LEVEL:   01.00     TIME:  12:02
TYPE:    FORT          USERID: CTJJC197    PAGE:  26 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8
REINIV=1./REN
FRINV=1./FR
FR2INV=FRINV*FRINV
RFRINV=FRINV*REINIV
RF2INV=REINIV*FR2INV
RN3INV=REINIV/3.
C
C
C
INITIALIZATIONS
EN=O.O
AAD=O.O
AAE=O.O
AAF=O.O
AAH=O.O
AHF=O.O
AHG=O.O
C
VOLUME INTEGRATIONS
DO 1 MMM=1,NL
C
DO 10 N=1,NPT
NN=NENL(MMM,N)
X(N)=XT(NN)
Y(N)=YT(NN)
U(N)=UT(NN)
V(N)=VT(NN)
P(N)=PRESS(NN,IK)
UR(N)=UUR(NN,IG)
VR(N)=VVR(NN,IG)
UI(N)=UII(NN,IG)
VI(N)=VVI(NN,IG)
CONTINUE
C
DO 20 K=1,4
DO 20 L=1,4
XI=ST(K)
ETA=ST(L)
ACOF=WS(K)*WS(L)
C
CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
CALL QUADR(AA,AB,X,Y,DX,DY,DXX,DXY,DYY,NPT)
C
YP=O.O
PRN=O.O
PRX=O.O
PRY=O.O
PRXX=O.O
PRXY=O.O
PRYY=O.O
UNN=O.O
UNX=O.O
UNY=O.O
C

```

MAIN2

DATE: 87/09/24
TIME: 12:02
PAGE: 27 OF 50

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

11 VNN=O.O
11 VNX=O.O
11 VNY=O.O
11 URN=O.O
11 URX=O.O
11 URY=O.O
11 VRN=O.O
11 VRX=O.O
11 VRY=O.O
11 UIN=O.O
11 UIX=O.O
11 UIY=O.O
11 VIN=O.O
11 VIX=O.O
11 VIY=O.O

C

11 DO 30 N=1,NPT
11 YP=Y*FI(N)*Y(N)
11 PRN=PRN+FI(N)*P(N)
11 PRX=PRX+DX(N)*P(N)
11 PRY=PRY+DY(N)*P(N)
11 PRXX=PRXX+DXX(N)*P(N)
11 PRXY=PRXY+DXY(N)*P(N)
11 PRYY=PRYY+DYY(N)*P(N)
11 UNN=UNN+FI(N)*U(N)
11 UNX=UNX+DX(N)*U(N)
11 UNY=UNY+DY(N)*U(N)
11 VNN=VNN+FI(N)*V(N)
11 VNX=VNX+DX(N)*V(N)
11 VNY=VNY+DY(N)*V(N)
11 URN=URN+FI(N)*UR(N)
11 URX=URX+DX(N)*UR(N)
11 URY=URY+DY(N)*UR(N)
11 VRN=VRN+FI(N)*VR(N)
11 VRX=VRX+DX(N)*VR(N)
11 VRY=VRY+DY(N)*VR(N)
11 UIN=UIN+FI(N)*UI(N)
11 UIX=UIX+DX(N)*UI(N)
11 UIY=UIY+DY(N)*UI(N)
11 VIN=VIN+FI(N)*VI(N)
11 VIX=VIX+DX(N)*VI(N)
11 VIY=VIY+DY(N)*VI(N)
11 CONTINUE

30

C=3.14159*Y*ACOF*DTA

C

11 EN=EN+C*2.O*PRN*PRN
11 AAD=AAD-C*(2.O*GAMMA+1.O)*PRN*(UNN*PRX+VNN*PRY)
11 AA=AAE+C*(-(UNN*PRX+VNN*PRY)*PRN
11 +2.O*(UNN*PRX+PRXX+VNN*PRY*PRY
11 +((UNN*PRX+VNN*PRY)*PRY)*FR21INV)
11 AA=AAE-C*((PRXX+PRXX+2.O*PRX*PRX+PRYY*PRY)*RF21INV
11 +FR*FR*PRN*PRN*RN3INV)
11 AHE=AHE+2.O*C*GAMMA*(UNN*UIN*PRXX+VNN*VIN*PRY

```

PROJECT: CTJC197      MEMBER: MAIN2      DATE: 87/09/24
GROUP:   STB1         LEVEL:   01.00     TIME: 12:02
TYPE:    FORT        USERID: CTJC197     PAGE: 28 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8
*          *          +((UNN*VIN+VNN*UIN)*PRXY)*FRINV
AHF=AHF-C*GAMMA*(UIX*PRXX+VIX*PRYY+(UIY+VIX)*PRXY)*RFRINV
AHG=AHG+2.O*C*GAMMA*(GAMMA-1.O)
*          *          *(2.O*(UNX*URX+VNX*VRX))
*          *          +(UNI+VNI)*(URY+VRX))*RENINV
CONTINUE
CONTINUE
RETURN
END
*          *          SUBROUTINE ELEUV(MMM,NPT,NGPT,XX,YY,UU,VV,PP,
RENU,DT,NENN,ANM,FNU,FNV,WS,ST,NEL)
LOCAL MATRICES FOR VELOCITIES
DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)
DIMENSION ANM(4,4),FNU(4),FNV(4),WS(4),ST(4)
DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4),
U(4),V(4),P(4),NENN(NEL,4)
*          *          RENINV=1./REN
DTINV=1./DT
DO 1 N=1,NPT
NN=NENN(MMM,N)
X(N)=XX(NN)
Y(N)=YY(NN)
U(N)=UU(NN)
V(N)=VV(NN)
P(N)=PP(NN)
CONTINUE
DO 2 N=1,NPT
FNU(N)=O.O
FNV(N)=O.O
DO 2 M=1,NPT
ANM(N,M)=O.O
CONTINUE
DO 300 K=1,4
DO 300 L=1,4
XI=ST(K)
ETA=ST(L)
ACDF=WS(K)*WS(L)
CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
SSU=O.O
SSV=O.O
SXP=O.O

```



```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      SYP=0.0
11      YP=0.0
11      C
11      DO 301 N=1,NPT
11      SSU=SSU+FI(N)*U(N)
11      SSV=SSV+FI(N)*V(N)
11      SXP=SXP+DX(N)*P(N)
11      SYP=SYP+DY(N)*P(N)
11      YP =YP +FI(N)*Y(N)
11      CONTINUE
11      301
11      C
11      C=ACOF*DTA*YP
11      C
11      DO 500 N=1,NPT
11      CFIN=C*FI(N)
11      FNU(N)=FNU(N)+CFIN*(SSU*DTINV-SXP)
11      FNV(N)=FNV(N)+CFIN*(SSV*DTINV-SYP)
11      DO 500 M=1,NPT
11      ANM(N,M)=ANM(N,M)+CFIN*(FI(M)*DTINV+SSU*DX(M)+SSV*DY(M))
11      +C*(DX(N)*DX(M)+DY(N)*DY(M))*RENINV
11      *
11      CONTINUE
11      500
11      CONTINUE
11      C
11      RETURN
11      END
11      C
11      C
11      SUBROUTINE ELEPR(MMM,NPT,NGPT,XX,YY,US,VS,
11      *      DT,BNM,GN,WS,ST,NEL,NENN)
11      LOCAL MATRICES FOR PRESSURE CORRECTIONS
11      C
11      DIMENSION XX(NGPT),YY(NGPT),US(NGPT),VS(NGPT)
11      DIMENSION BNM(4,4),GN(4),WS(4),ST(4),NENN(NEL,4)
11      DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4),U(4),V(4)
11      C
11      DTINV=1./DT
11      DO 1 N=1,NPT
11      NN=NENN(MMM,N)
11      X(N)=XX(NN)
11      Y(N)=YY(NN)
11      U(N)=US(NN)
11      V(N)=VS(NN)
11      CONTINUE
11      1
11      C
11      DO 2 N=1,NPT
11      GN(N)=0.0
11      DO 2 M=1,NPT
11      BNM(N,M)=0.0
11      CONTINUE
11      2
11      C
11      DO 300 K=1,4
11      DO 300 L=1,4
11      XI=ST(K)

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 30 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)
1 C
11      CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
1 C
11      SXU=O.O
11      SYV=O.O
11      YP =O.O
1 C
11      DO 301 N=1,NPT
11      SXU=SXU+DX(N)*U(N)
11      SYV=SYV+DY(N)*V(N)
11      YP =YP +FI(N)*Y(N)
11      CONTINUE
1 301
1 C
11      C=ACOF*DTA*YP
1 C
11      DO 500 N=1,NPT
11      GN(N)=GN(N)-C*FI(N)*(SXU+SYV)*DTINV
11      DO 500 M=1,NPT
11      BNM(N,M)=BNM(N,M)+C*(DX(N)*DX(M)+DY(N)*DY(M))
11      CONTINUE
1 500
1 300
1 C
11      RETURN
11      END
11
11      *
11      SUBROUTINE ELEAC(MMM,NPT,NGPT,XX,YY,DPP,CNM,
11      HNU,HNV,WS,ST,NEL,NENN)
11
11      LOCAL MATRICES FOR ACCELERATIONS
11
11      DIMENSION XX(NGPT),YY(NGPT),DPP(NGPT),NENN(NEL,4)
11      DIMENSION CNM(4,4),HNU(4),HNV(4),WS(4),ST(4)
11      DIMENSION X(4),Y(4),DP(4),FI(4),DX(4),DY(4),AA(4),AB(4)
11
11      DO 1 N=1,NPT
11      NW=NENN(MMM,N)
11      X(N)=XX(NN)
11      Y(N)=YY(NN)
11      DP(N)=DPP(NN)
11      CONTINUE
1 1
1 C
11      DO 2 N=1,NPT
11      HNU(N)=O.O
11      HNV(N)=O.O
11      DO 2 M=1,NPT
11      CNM(N,M)=O.O
11      CONTINUE
1 2
1 C
11      DO 300 K=1,4
11      DO 300 L=1,4
11      XI=ST(K)

```

PROJECT: CTJUC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJUC197

DATE: 87/09/24
TIME: 12:02
PAGE: 31 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)
11      C
11      CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
11      C
11      SDPX=0.0
11      SDPY=0.0
11      YP =0.0
11      C
11      DO 310 N=1,NPT
11      SDPX=SDPX+DX(N)*DP(N)
11      SDPY=SDPY+DY(N)*DP(N)
11      YP =YP +FI(N)*Y(N)
11      CONTINUE
11      310
11      C
11      C=ACOF*DTA*YP
11      C
11      DO 500 N=1,NPT
11      CFIN=C*FI(N)
11      HNJ(N)=HNJ(N)-CFIN*SDPX
11      HNV(N)=HNV(N)-CFIN*SDPY
11      DO 500 M=1,NPT
11      CNM(N,M)=CNM(N,M)+CFIN*FI(M)
11      CONTINUE
11      500
11      300
11      C
11      RETURN
11      END
11      C
11      SUBROUTINE ELEMP(MMM,NPT,ANM,BNM,WS,ST,NL,NT,NENL,
11      XT,YT)
11      C
11      DIMENSION XT(NT),YT(NT)
11      DIMENSION ANM(4,4),BNM(4,4),WS(4),ST(4),NENL(NL,4)
11      DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4)
11      C
11      DO 100 N=1,NPT
11      NN=NENL(MMM,N)
11      X(N)=XT(NN)
11      Y(N)=YT(NN)
11      CONTINUE
11      100
11      C
11      DO 110 I=1,NPT
11      DO 110 J=1,NPT
11      ANM(I,J)=0.0
11      BNM(I,J)=0.0
11      CONTINUE
11      110
11      C
11      DO 300 K=1,4
11      DO 300 L=1,4
11      XI=ST(K)
11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)

```

```

PROJECT: CTJC197      MEMBER: MAIN2      DATE: 87/09/24
GROUP:   STB1         LEVEL:   O1.OO     TIME: 12:02
TYPE:    FORT        USERID: CTJC197     PAGE: 32 OF 50

-----1-----2-----3-----4-----5-----6-----7-----+-----8
START COL

1 C          CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DIA,AA,AB)
11 C
1 C          YP=O.O
11 C
11 DO 310 N=1,NPT
11 YP=YF+FI(N)*V(N)
11 CONTINUE
1 310
1 C
11 C=BCOF*DTA*YP
11 C
11 DO 500 N=1,NPT
11 CFIN=C*FI(N)
11 DO 500 M=1,NPT
11 ANM(N,M)=ANM(N,M)+C*(DX(N)*DX(M)+DY(N)*DY(M))
11 BNM(N,M)=BNM(N,M)+CFIN*FI(M)
11 CONTINUE
1 500
1 300
1 C
11 RETURN
11 END
11 C
1 C
1 C
11 SUBROUTINE ELEVR(MMM,NPT,ANM,BNM,WS,ST,REN,NL,NT,NENL,
*           XT,YT,UT,VT)
11 C
11 C          LOCAL ELEMENT FOR VORTICAL EIGENMODES
11 C
11 DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11 DIMENSION X(4),Y(4),U(4),V(4),ANM(4,4,4,4),BNM(4,4,4,4),
*           WS(4),ST(4),PI(4,4),DPX(4,4),DPY(4,4),
*           DPXX(4,4),DPXY(4,4),DPYY(4,4),NENL(NL,4)
11 C
11 RENINV=.1./REN
11 C
11 DO 100 N=1,NPT
11 NN=NENL(MMM,N)
11 X(N)=XT(NN)
11 Y(N)=YT(NN)
11 U(N)=UT(NN)
11 V(N)=VT(NN)
11 CONTINUE
1 100
1 C
11 DO 110 L=1,4
11 DO 110 N=1,NPT
11 DO 110 LL=1,4
11 DO 110 M=1,NPT
11 ANM(L,LL,N,M)=O.O
11 BNM(L,LL,N,M)=O.O
11 CONTINUE
1 110
1 C
11 DA=ABS(X(2)-X(1))* .5
11 DB=ABS(Y(4)-Y(1))* .5
11 C

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 33 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      DO 300 K=1.4
11      DO 300 L=1.4
11      XI=ST(K)
11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)
11      C
11      CALL HERMT(XI,ETA,DA,DB,PI,DPX,DPY,DPXX,DPXY,DPYY)
11      C
11      SU=0.0
11      SV=0.0
11      SUX=0.0
11      SUY=0.0
11      SVX=0.0
11      SVY=0.0
11      SUXX=0.0
11      SUXY=0.0
11      SUYY=0.0
11      SVXX=0.0
11      SVXY=0.0
11      SVYY=0.0
11      YP=0.0
11      C
11      DO 310 N=1,NPT
11      SU=SU+PI(1,N)*U(N)
11      SV=SV+PI(1,N)*V(N)
11      SUX=SUX+DPX(1,N)*U(N)
11      SUY=SUY+DPY(1,N)*U(N)
11      SVX=SVX+DPX(1,N)*V(N)
11      SVY=SVY+DPY(1,N)*V(N)
11      SUXX=SUXX+DPXX(1,N)*U(N)
11      SUXY=SUXY+DPXY(1,N)*U(N)
11      SUYY=SUY+DPYY(1,N)*U(N)
11      SVXX=SVXX+DPXX(1,N)*V(N)
11      SVXY=SVXY+DPXY(1,N)*V(N)
11      SVYY=SVYY+DPYY(1,N)*V(N)
11      YP=YP+PI(1,N)*Y(N)
11      CONTINUE
11      310
11      C
11      C=ACOF*DA*DB*YP
11      C
11      DO 500 IL=1.4
11      DO 500 N=1,NPT
11      DO 500 JL=1.4
11      DO 500 M=1,NPT
11      ANM(IL,JL,N,M)=ANM(IL,JL,N,M)+C*(
11      PI(IL,N)*(SVXX*DPY(JL,M)-SVXY*DPX(JL,M)
11      -SUXY*DPY(JL,M)+SUY*DPX(JL,M))
11      +(SU*DPX(IL,N)+SV*DPY(IL,N))*(DPXX(JL,M)+DPYY(JL,M))
11      -(DPXX(IL,N)*DPXX(JL,M)+2.0*DPXY(IL,N)*DPXY(JL,M)
11      +DPYY(IL,N)*DPYY(JL,M))*RENINV)
11      BNM(IL,JL,N,M)=BNM(IL,JL,N,M)+C*(
11      DPX(IL,N)*DPX(JL,M)+DPY(IL,N)*DPY(JL,M))
11      CONTINUE
11      500
11      CONTINUE

```

MAIN2

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 34 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
1 C
11 RETURN
11 END
1 C
1 C
1 C
1 C
11 SUBROUTINE ADJUST(NB,NT,NBX,A,UNB,F,NBW1,NBWT)
1 C
1 C
1 C
1 C
11 ADJUSTMENT OF BOUNDARY CONDITIONS FOR MEAN VELOCITY FIELDS
1 C
11 DIMENSION NBX(NB),UNB(NB)
11 DIMENSION A(NT,NBWT),F(NT)
1 C
11 DO 1 I=1,NB
11 ND=NBX(I)
11 DO 2 J=1,NBWT
11 A(ND,J)=0.0
11 DO 3 J=1,NT
11 NX1=(ND-1)+NBWT
11 IF(NX1.LE.0.OR.NX1.GT.NBWT) GO TO 3
11 F(J)=F(J)-A(J,NX1)*UNB(I)
11 A(J,NX1)=0.0
11 CONTINUE
11 A(ND,NBW1)=1.0
11 F(ND)=UNB(I)
11 CONTINUE
1 C
11 RETURN
11 END
1 C
1 C
11 SUBROUTINE GAUSSU(A,B,X,N,NBW1,NBWT)
1 C
1 C
1 C
1 C
11 SOLVER OF LINEAR EQUATIONS WITH BAND MATRIX
1 C
11 DIMENSION A(N,NBWT),B(N),X(N)
1 C
11 NM1=N-1
1 C
11 DO 5 I=1,NM1
11 IP1=I+1
11 DO 6 K=IP1,N
11 II=I-K+NBW1
11 IF(II.LE.0 .OR. II.GT.NBWT) GO TO 6
11 FACT=-A(K,II)/A(I,NBW1)
11 IF(FACT.EQ.0.0) GO TO 6
11 A(K,II)=0.0
11 DO 7 J=IP1,N
11 JJ=J-I+NBW1
11 IF(JJ.LE.0 .OR. JJ.GT.NBWT) GO TO 7
11 JJ=J-K+NBW1
11 IF(JJ.LE.0 .OR. JJ.GT.NBWT) GO TO 7
11 A(K,JJ)=A(K,JJ)+FACT*A(I,JJ)
11 CONTINUE
11 7

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 35 OF 50

MAIN2

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
11      B(K)=B(K)+FACT*B(I)
1        CONTINUE
1 6      CONTINUE
1 5
1 C
1 C
11      X(N)=B(N)/A(N,NBW1)
11      NP1=N+1
11      DO 2 K=1,NM1
11      SUM=0.0
11      NMK=N-K
11      DO 3 J=1,K
11      JJ=(NP1-J)-NMK+NBW1
11      IF(JJ.LE.0 .OR. JJ.GT.NBWT) GO TO 3
11      SUM=SUM+A(NMK,JJ)*X(NP1-J)
1 3      CONTINUE
11      X(NMK)=(B(NMK)-SUM)/A(NMK,NBW1)
1 2      CONTINUE
1 C      RETURN
11      END
11
1 C
1 C
1 C
1 C
7      SUBROUTINE GAUSS(NGG,W,ST)
7      DIMENSION W(NGG),ST(NGG)
7 C
7      IF(NGG.EQ.1) GO TO 10
7      IF(NGG.EQ.2) GO TO 20
7      IF(NGG.EQ.3) GO TO 30
7      IF(NGG.EQ.4) GO TO 40
7      IF(NGG.EQ.5) GO TO 50
7      IF(NGG.EQ.6) GO TO 60
1 C
2 10     W(1)=2.0
2      ST(1)=0.0
7      GO TO 70
1 C
2 20     W(1) = 1.0
2      W(2) = W(1)
7      ST(1) = -0.577350269
7      ST(2) = -ST(1)
7      GO TO 70
1 C
2 30     W(1) = 0.5555555555
2      W(2) = 0.8888888888
7      W(3) = W(1)
7      ST(1) = -0.7745966692
7      ST(2) = 0.0
7      ST(3) = -ST(1)
7      GO TO 70
1 C
2 40     W(1) = 0.3478548451
2      W(2) = 0.6521451548
7

```

MAIN2

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT

MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197

DATE: 87/09/24
 TIME: 12:02
 PAGE: 36 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

7 W(3) = W(2)
 7 W(4) = W(1)
 7 ST(1) = -0.8611363115
 7 ST(2) = -0.3399810435
 7 ST(3) = -ST(2)
 7 ST(4) = -ST(1)
 7 GO TO 70

1 C
 2 50 W(1) = 0.2369268850
 7 W(2) = 0.478628674
 7 W(3) = 0.5688888888
 7 W(4) = W(2)
 7 W(5) = W(1)
 7 ST(1) = -0.9061798459
 7 ST(2) = -0.5384693101
 7 ST(3) = 0.0
 7 ST(4) = -ST(2)
 7 ST(5) = -ST(1)
 7 GO TO 70

1 C
 2 60 W(1) = 0.1713244923
 7 W(2) = 0.3607615730
 7 W(3) = 0.4679139345
 7 W(4) = W(3)
 7 W(5) = W(2)
 7 W(6) = W(1)
 7 ST(1) = -0.9324695142
 7 ST(2) = -0.6612093864
 7 ST(3) = -0.2386191860
 7 ST(4) = -ST(3)
 7 ST(5) = -ST(2)
 7 ST(6) = -ST(1)

1 C 70 CONTINUE

1 C
 7 RETURN
 7 END

SUBROUTINE INTER(XX,YY,NPT,X,Y,DX,DY,FT,DTA,AA,AB)
 LINEAR INTERPOLATION FUNCTIONS AND THEIR FIRST DERIVATIVES
 DIMENSION X(NPT),Y(NPT),DX(NPT),DY(NPT),FT(NPT)
 DIMENSION AA(NPT),AB(NPT),DTJ(2,2)

FT(1)=0.25*(1.0-XX)*(1.0-YY)
 FT(2)=0.25*(1.0+XX)*(1.0-YY)
 FT(3)=0.25*(1.0+XX)*(1.0+YY)
 FT(4)=0.25*(1.0-XX)*(1.0+YY)
 AA(1)=0.25*(-1.0+YY)
 AA(2)=0.25*(1.0-YY)

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 37 OF 50

START COL 1 2 3 4 5 6 7 8

1 C AA(3)=0.25*(1.0+YY)
1 C AA(4)=0.25*(-1.0-YY)

1 C AB(1)=0.25*(-1.0+XX)
1 C AB(2)=0.25*(-1.0-XX)
1 C AB(3)=0.25*(1.0+XX)
1 C AB(4)=0.25*(1.0-XX)

1 C XXP1=XX+1.
7 XXM1=XX-1.
7 YYP1=YY+1.
7 YYM1=YY-1.

1 C AA(1)=.25*YYM1
7 AA(2)=-AA(1)
7 AA(3)=.25*YYP1
7 AA(4)=-AA(3)

1 C AB(1)=.25*XXM1
7 AB(3)=.25*XXP1
7 AB(2)=-AB(3)
7 AB(4)=-AB(1)

1 C FT(1)=AB(1)*YYM1
7 FT(2)=AB(2)*YYM1
7 FT(3)=AB(3)*YYP1
7 FT(4)=AB(4)*YYP1

1 C DO 4 I=1,2
11 DO 4 J=1,2
11 DTJ(I,J)=0.0

1 C DO 5 N=1,NPT
11 DTJ(1,1)=DTJ(1,1)+AA(N)*X(N)
11 DTJ(1,2)=DTJ(1,2)+AA(N)*Y(N)
11 DTJ(2,1)=DTJ(2,1)+AB(N)*X(N)
11 DTJ(2,2)=DTJ(2,2)+AB(N)*Y(N)

1 C DTA=DTJ(1,1)*DTJ(2,2)-DTJ(1,2)*DTJ(2,1)
11 DTAINV=1./DTA

1 C DO 7 N=1,NPT
11 DX(N)=(DTJ(2,2)*AA(N)-DTJ(1,2)*AB(N))*DTAINV
11 DY(N)=(-DTJ(2,1)*AA(N)+DTJ(1,1)*AB(N))*DTAINV
11 CONTINUE

1 C RETURN
11 END

SUBROUTINE QUADR(AA,AB,X,Y,DX,DY,DXX,DXY,DYY,NPT)
SECOND DERIVATIVES OF INTERPOLATION FUNCTIONS


```

START
COL 1-----2-----3-----4-----5-----6-----7-----8
2 8 CONTINUE
1 C
11 D11=(DXX1*DYV1+DXX1*DYX1)*DYV1*DYV1-2.*DYX1*DYV1+DXX1*DYV1+DYV1*DYV1
11 D12=2.*DYX1*DYV1+DYV1*DYV1-2.*DXX1*DYX1+DYV1*DYV1
11 D13=2.*DXX1*DYX1+DYV1*DYV1-DXX1*DYX1*(DXX1*DYV1+DYX1*DYX1)
11 D21=DXX1*DYX1+DYV1*DYX1-DXX1*DYX1*DYV1+DYV1
11 D22=DXX1*DXX1+DYV1*DYV1-DXX1*DYX1*DYX1+DYX1
11 D23=DXX1*DYX1+DXX1*DYX1-DXX1*DYX1*DYX1+DYX1
11 D31=2.*DXX1*DYX1+DYV1*DYV1-DXX1*DYX1*(DXX1*DYV1+DYX1*DYX1)
11 D32=DXX1*DYX1+DXX1*DYX1-DXX1*DYX1*DYV1+DYV1
11 D33=DXX1*DXX1*(DXX1*DYV1+DYX1*DXX1)-2.*DXX1*DYX1+DXX1*DYX1
1 C
1 C
DO 9 N=1,NPT
DXX(N)=(D11*DUMXX(N)+D12*DUMXY(N)+D13*DUMYY(N))*DDDINV
DXY(N)=(D21*DUMXX(N)+D22*DUMXY(N)+D23*DUMYY(N))*DDDINV
DYY(N)=(D31*DUMXX(N)+D32*DUMXY(N)+D33*DUMYY(N))*DDDINV
2 9 CONTINUE
1 C
1 C
RETURN
END
SUBROUTINE HERMT(XI,ETA,DA,DB,PI,DPX,DPY,DPXX,DPXY,DPYY)
HERMITE POLYNOMIAL INTERPOLATION FUNCTIONS
DIMENSION PI(4,4),DPX(4,4),DPY(4,4),DPXX(4,4),DPXY(4,4),
DPYY(4,4)
DAINV4=.25/DA
DBINV4=.25/DB
DA2INV4=DAINV4/DA
DB2INV4=DBINV4/DB
F1X=(2.-3.*XI+XI*XI)*.25
F2X=(2.+3.*XI-XI*XI)*.25
G1X=DA*(1.-XI-XI*XI+XI*XI)*.25
G2X=DA*(-1.-XI+XI*XI+XI*XI)*.25
F1Y=(2.-3.*ETA+ETA*ETA)*.25
F2Y=(2.+3.*ETA-ETA*ETA)*.25
G1Y=DB*(1.-ETA-ETA*ETA+ETA*ETA)*.25
G2Y=DB*(-1.-ETA+ETA*ETA+ETA*ETA)*.25
DF1X=(-3.+3.*XI*XI)*DAINV4
DF2X=(3.-3.*XI*XI)*DAINV4
DG1X=(-1.-2.*XI+3.*XI*XI)*.25
DG2X=(-1.+2.*XI+3.*XI*XI)*.25
DF1Y=(-3.+3.*ETA*ETA)*DBINV4
DF2Y=(3.-3.*ETA*ETA)*DBINV4
DG1Y=(-1.-2.*ETA+3.*ETA*ETA)*.25
DG2Y=(-1.+2.*ETA+3.*ETA*ETA)*.25
DOF1X=6.*XI*DA2INV4

```

PROJECT: CTJUC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJUC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 40 OF 50
 MAIN2

START COL 1 2 3 4 5 6 7 8
 DDF2X=-6.*XI*DA21N4
 DDG1X=(-2.+6.*XI)*DAINV4
 DDG2X=(2.+6.*XI)*DAINV4
 C
 DDF1Y=6.*ETA*DB21N4
 DDF2Y=-6.*ETA*DB21N4
 DDG1Y=(-2.+6.*ETA)*DBINV4
 DDG2Y=(2.+6.*ETA)*DBINV4
 C
 PI(1,1)=F1X*F1Y
 PI(1,2)=F2X*F1Y
 PI(1,3)=F2X*F2Y
 PI(1,4)=F1X*F2Y
 PI(2,1)=G1X*F1Y
 PI(2,2)=G2X*F1Y
 PI(2,3)=G2X*F2Y
 PI(2,4)=G1X*F2Y
 PI(3,1)=F1X*G1Y
 PI(3,2)=F2X*G1Y
 PI(3,3)=F2X*G2Y
 PI(3,4)=F1X*G2Y
 PI(4,1)=G1X*G1Y
 PI(4,2)=G2X*G1Y
 PI(4,3)=G2X*G2Y
 PI(4,4)=G1X*G2Y
 C
 DPX(1,1)=DF1X*F1Y
 DPX(1,2)=DF2X*F1Y
 DPX(1,3)=DF2X*F2Y
 DPX(1,4)=DF1X*F2Y
 DPX(2,1)=DG1X*F1Y
 DPX(2,2)=DG2X*F1Y
 DPX(2,3)=DG2X*F2Y
 DPX(2,4)=DG1X*F2Y
 DPX(3,1)=DF1X*G1Y
 DPX(3,2)=DF2X*G1Y
 DPX(3,3)=DF2X*G2Y
 DPX(3,4)=DF1X*G2Y
 DPX(4,1)=DG1X*G1Y
 DPX(4,2)=DG2X*G1Y
 DPX(4,3)=DG2X*G2Y
 DPX(4,4)=DG1X*G2Y
 C
 DPY(1,1)=F1X*DF1Y
 DPY(1,2)=F2X*DF1Y
 DPY(1,3)=F2X*DF2Y
 DPY(1,4)=F1X*DF2Y
 DPY(2,1)=G1X*DF1Y
 DPY(2,2)=G2X*DF1Y
 DPY(2,3)=G2X*DF2Y
 DPY(2,4)=G1X*DF2Y
 DPY(3,1)=F1X*DG1Y
 DPY(3,2)=F2X*DG1Y
 DPY(3,3)=F2X*DG2Y

PROJECT: CTJC197
GROUP: STB1
TYPE: FORT

MEMBER: MAIN2
LEVEL: 01.00
USERID: CTJC197

DATE: 87/09/24
TIME: 12:02
PAGE: 41 OF 50

MAIN2

START	COL	1	2	3	4	5	6	7	8
11		DPY(3,4)=F1X*DG2Y							
11		DPY(4,1)=G1X*DG1Y							
11		DPY(4,2)=G2X*DG1Y							
11		DPY(4,3)=G2X*DG2Y							
11		DPY(4,4)=G1X*DG2Y							
11	C								
11		DPXX(1,1)=DDF1X*F1Y							
11		DPXX(1,2)=DDF2X*F1Y							
11		DPXX(1,3)=DDF2X*F2Y							
11		DPXX(1,4)=DDF1X*F2Y							
11		DPXX(2,1)=DDG1X*F1Y							
11		DPXX(2,2)=DDG2X*F1Y							
11		DPXX(2,3)=DDG2X*F2Y							
11		DPXX(2,4)=DDG1X*F2Y							
11		DPXX(3,1)=DDF1X*G1Y							
11		DPXX(3,2)=DDF2X*G1Y							
11		DPXX(3,3)=DDF2X*G2Y							
11		DPXX(3,4)=DDF1X*G2Y							
11		DPXX(4,1)=DDG1X*G1Y							
11		DPXX(4,2)=DDG2X*G1Y							
11		DPXX(4,3)=DDG2X*G2Y							
11		DPXX(4,4)=DDG1X*G2Y							
11	C								
11		DPYY(1,1)=F1X*DDF1Y							
11		DPYY(1,2)=F2X*DDF1Y							
11		DPYY(1,3)=F2X*DDF2Y							
11		DPYY(1,4)=F1X*DDF2Y							
11		DPYY(2,1)=G1X*DDF1Y							
11		DPYY(2,2)=G2X*DDF1Y							
11		DPYY(2,3)=G2X*DDF2Y							
11		DPYY(2,4)=G1X*DDF2Y							
11		DPYY(3,1)=F1X*DDG1Y							
11		DPYY(3,2)=F2X*DDG1Y							
11		DPYY(3,3)=F2X*DDG2Y							
11		DPYY(3,4)=F1X*DDG2Y							
11		DPYY(4,1)=G1X*DDG1Y							
11		DPYY(4,2)=G2X*DDG1Y							
11		DPYY(4,3)=G2X*DDG2Y							
11		DPYY(4,4)=G1X*DDG2Y							
11	C								
11		DPXY(1,1)=DF1X*DF1Y							
11		DPXY(1,2)=DF2X*DF1Y							
11		DPXY(1,3)=DF2X*DF2Y							
11		DPXY(1,4)=DF1X*DF2Y							
11		DPXY(2,1)=DG1X*DF1Y							
11		DPXY(2,2)=DG2X*DF1Y							
11		DPXY(2,3)=DG2X*DF2Y							
11		DPXY(2,4)=DG1X*DF2Y							
11		DPXY(3,1)=DF1X*DG1Y							
11		DPXY(3,2)=DF2X*DG1Y							
11		DPXY(3,3)=DF2X*DG2Y							
11		DPXY(3,4)=DF1X*DG2Y							
11		DPXY(4,1)=DG1X*DG1Y							
11		DPXY(4,2)=DG2X*DG1Y							

START	COL	1	2	3	4	5	6	7	8
11		DPXY(4,3)=DG2X+DG2Y							530970
11		DPXY(4,4)=DG1X+DG2Y							530980
1	C								530990
11		RETURN							531000
11		END							531010
7		SUBROUTINE CONVRT							531020
6	C	\$(N, A, NA, B, NB, X, NX)							531030
1		COMPLEX A(NA,N)							531040
7		COMPLEX B(NB,N)							531050
7		COMPLEX W							531060
7		COMPLEX X(NX,N)							531070
7		COMPLEX Y							531080
7		COMPLEX Z							531090
1	C	REAL C							531100
7		REAL D							531110
1	C	INTEGER I							531120
7		INTEGER II							531130
7		INTEGER IMJ							531140
7		INTEGER IM1							531150
7		INTEGER IP1							531160
7		INTEGER J							531170
7		INTEGER JM2							531180
7		INTEGER JP1							531190
7		INTEGER K							531200
7		INTEGER N							531210
7		INTEGER NA							531220
7		INTEGER NB							531230
7		INTEGER NM1							531240
7		INTEGER NM2							531250
7		INTEGER NX							531260
1	C	LUWT = 6							531270
7		NM1 = N - 1							531280
7		DO 80 I=1,NM1							531290
7		D = 0.0							531300
7		IP1 = I + 1							531310
7		DO 10 K=IP1,N							531320
7		Y = B(K,I)							531330
7		C = ABS(REAL(Y)) + ABS(AIMAG(Y))							531340
7		IF(C.LE.D) GO TO 9							531350
7		D = C							531360
7		II = K							531370
5		9 CONTINUE							531380
10		10 CONTINUE							531390
7		IF(D.EQ.O.O) GO TO 78							531400
7		Y = B(I,I)							531410
7		IF(D.LE.ABS(REAL(Y)) + ABS(AIMAG(Y))) GO TO 40							531420
7		DO 20 J=1,N							531430
7		Y = A(I,J)							531440
7		A(I,J) = A(II,J)							531450
7		A(II,J) = Y							

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 43 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8
4 20 CONTINUE 531460
7 DO 30 J=1,N 531470
7 Y = B(I,J) 531480
7 B(I,J) = B(II,J) 531490
7 B(II,J) = Y 531500
4 30 CONTINUE 531510
4 40 CONTINUE 531520
7 DO 70 J=IP1,N 531530
7 Y = B(J,I)/B(I,I) 531540
7 IF( REAL(Y).EQ.O.O .AND. AIMAG(Y).EQ.O.O ) GO TO 68 531550
7 DO 50 K=1,N 531560
7 A(J,K) = A(J,K) - Y*A(I,K) 531570
4 50 CONTINUE 531580
7 DO 60 K=IP1,N 531590
7 B(J,K) = B(J,K) - Y*B(I,K) 531600
4 60 CONTINUE 531610
4 68 CONTINUE 531620
4 70 CONTINUE 531630
7 B(IP1,I) = CMPLX(O.O.O.O) 531640
4 78 CONTINUE 531650
4 80 CONTINUE 531660
1 1 C 53167
7 DO 100 I=1,N 531680
7 DO 90 J=1,N 531690
7 X(I,J) = CMPLX(O.O.O.O) 531700
4 90 CONTINUE 531710
7 X(I,I) = CMPLX(1.O.O.O) 531720
3 100 CONTINUE 531730
1 1 C 531740
7 NM2 = N - 2 531750
7 IF( NM2.LT.1 ) GO TO 270 531760
7 DO 260 J=1,NM2 531770
7 JM2 = NM1 - J 531780
7 JP1 = J + 1 531790
7 DO 250 II=1,JM2 531800
7 I = N + 1 - II 531810
7 IM1 = I - 1 531820
7 IMJ = I - J 531830
1 1 C 531840
7 W = A(I,J) 531850
7 Z = A(IM1,J) 531860
7 IF( ABS(REAL(W)) + ABS(AIMAG(W)).LE. 531870
6 $ ABS(REAL(Z)) + ABS(AIMAG(Z)) ) GO TO 140 531880
7 DO 120 K=J,N 531890
7 Y = A(I,K) 531900
7 A(I,K) = A(IM1,K) 531910
7 A(IM1,K) = Y 531920
3 120 CONTINUE 531930
7 DO 130 K=IM1,N 531940
7 Y = B(I,K) 531950
7 B(I,K) = B(IM1,K) 531960
7 B(IM1,K) = Y 531970
3 130 CONTINUE 531980
3 140 CONTINUE 531990

```

PROJECT: CTJC197
 GROUP: STB1
 TYPE: FORT
 MEMBER: MAIN2
 LEVEL: 01.00
 USERID: CTJC197
 DATE: 87/09/24
 TIME: 12:02
 PAGE: 44 OF 50

MAIN2

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
1 C
7 Z = A(I,J)
7 IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O ) GO TO 170
7 Y = Z/A(IM1,J)
7 DO 150 K=JP1,N
7 A(I,K) = A(I,K) - Y*A(IM1,K)
3 150 CONTINUE
7 DO 160 K=IM1,N
7 B(I,K) = B(I,K) - Y*B(IM1,K)
3 160 CONTINUE
3 170 CONTINUE
1 C
7 W = B(I,IM1)
7 Z = B(I,I)
7 IF( ABS(REAL(W)) + ABS(AIMAG(W)) .LE.
6 $ ABS(REAL(Z)) + ABS(AIMAG(Z)) ) GO TO 210
7 DO 180 K=1,I
7 Y = B(K,I)
7 B(K,I) = B(K,IM1)
7 B(K,IM1) = Y
3 180 CONTINUE
7 DO 190 K=1,N
7 Y = A(K,I)
7 A(K,I) = A(K,IM1)
7 A(K,IM1) = Y
3 190 CONTINUE
7 DO 200 K=IMJ,N
7 Y = X(K,I)
7 X(K,I) = X(K,IM1)
7 X(K,IM1) = Y
3 200 CONTINUE
3 210 CONTINUE
1 C
7 Z = B(I,IM1)
7 IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O ) GO TO 249
7 Y = Z/B(I,I)
7 DO 220 K=1,IM1
7 B(K,IM1) = B(K,IM1) - Y*B(K,I)
3 220 CONTINUE
7 B(I,IM1) = CMPLX(O.O,O.O)
7 DO 230 K=1,N
7 A(K,IM1) = A(K,IM1) - Y*A(K,I)
3 230 CONTINUE
7 DO 240 K=IMJ,N
7 X(K,IM1) = X(K,IM1) - Y*X(K,I)
3 240 CONTINUE
3 249 CONTINUE
1 C
3 250 CONTINUE
7 A(JP1+1,J) = CMPLX(O.O,O.O)
3 260 CONTINUE
3 270 CONTINUE
1 C
7 RETURN
  
```

532000
 532010
 532020
 532030
 532040
 532050
 53767
 532070
 532080
 532090
 532100
 532110
 532120
 532130
 532140
 532150
 532160
 532170
 532180
 532190
 532200
 532210
 532220
 532230
 532240
 532250
 532260
 532270
 532280
 532290
 532300
 532310
 532320
 532330
 532340
 532350
 532360
 532370
 532380
 538320
 532400
 532410
 532420
 532430
 532440
 532450
 532460
 532470
 532480
 532490
 532500
 532510
 532520
 532530

START	COL	1	2	3	4	5	6	7	8
7		END							532540
7		SUBROUTINE SOLVE							532550
6		\$(N, A, NA, B, NB, X, NX, ITER, EIGA, EIGB)							532560
1	C								532570
7		COMPLEX S							532580
7		COMPLEX W							532590
7		COMPLEX Y							532600
7		COMPLEX Z							532610
7		COMPLEX A(NA,N)							532620
7		COMPLEX B(NB,N)							532630
7		COMPLEX X(NX,N)							532640
7		COMPLEX EIGA(N)							532650
7		COMPLEX EIGB(N)							532660
7		COMPLEX ANNM1							53267
7		COMPLEX ALFM							532680
7		COMPLEX BETM							532690
7		COMPLEX D							532700
7		COMPLEX SL							532710
7		COMPLEX DEN							532720
7		COMPLEX NUM							532730
7		COMPLEX ANM1M1							532740
1	C								532750
7		REAL DO							532760
7		REAL D1							532770
7		REAL D2							532780
7		REAL EO							532790
7		REAL E1							532800
7		REAL C							532810
7		REAL EPSA							532820
7		REAL EPSB							532830
7		REAL SS							532840
7		REAL R							532850
7		REAL ANORM							532860
7		REAL BNORM							532870
7		REAL ANI							532880
7		REAL BNI							532890
1	C								532900
7		INTEGER ITER(N)							532910
1	C								532920
7		NN = N							532930
7		ANORM = O.O							532940
7		BNORM = O.O							532950
7		DO 30 I=1,N							532960
7		ANI = O.O							532970
7		IF(1.EQ.1)							532980
7		Y = A(I,I-1)							532990
7		ANI = ANI + ABS(REAL(Y)) + ABS(AIMAG(Y))							533000
4		10 CONTINUE							533010
7		BNI = O.O							533020
7		DO 20 J=1,N							533030
7		ANI = ANI + ABS(REAL(A(I,J))) + ABS(AIMAG(A(I,J)))							533040
7		BNI = BNI + ABS(REAL(B(I,J))) + ABS(AIMAG(B(I,J)))							533050
4		20 CONTINUE							533060
7		IF(ANI.GT.ANORM) ANORM = ANI							533070

PROJECT: CTJJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJJC197 PAGE: 46 OF 50

```

START COL 1-----2-----3-----4-----5-----6-----7-----8
7      IF( BNI.GT.BNORM )      BNORM = BNI      533080
4      30 CONTINUE
1      C
7      IF( ANORM.EQ.O.O )      ANORM = 1.0      533090
7      IF( BNORM.EQ.O.O )      BNORM = 1.0      533100
7      EPSA = ANORM      533110
7      EPSB = BNORM      533120
4      40 CONTINUE      533130
7      EPSA = EPSA/2.0      533140
7      EPSB = EPSB/2.0      533150
7      C = ANORM + EPSA      533160
7      IF( C.GT.ANORM )      GO TO 40      533170
7      IF( N.LE.1 )      GO TO 320      533180
4      50 CONTINUE      533190
7      ITS = 0      533200
7      NM1 = NN - 1      533210
4      60 CONTINUE      533220
7      D2 = ABS(REAL(A(NN,NN))) + ABS(AIMAG(A(NN,NN)))      533230
7      DO 70 LB=2,NN      533240
7      L = NN + 2 - LB      533250
7      SS = D2      533260
7      Y = A(L-1,L-1)      533270
7      D2 = ABS(REAL(Y)) + ABS(AIMAG(Y))      533280
7      SS = SS + D2      533290
7      Y = A(L,L-1)      533300
7      R = SS + ABS(REAL(Y)) + ABS(AIMAG(Y))      533310
7      IF( R.EQ.SS )      GO TO 80      533320
4      70 CONTINUE      533330
7      L = 1      533340
4      80 CONTINUE      533350
7      IF( L.EQ.NN )      GO TO 320      533360
7      IF( ITS.LT.30 )      GO TO 90      533370
7      ITER(NN) = -1      533380
7      IF( ABS(REAL(A(NN,NM1))) + ABS(AIMAG(A(NN,NM1))) .GT.      533390
6      $.8*ABS(REAL(ANM1)) + ABS(AIMAG(ANM1)) )      GO TO 999      533400
4      90 CONTINUE      533410
7      IF( ITS.EQ.10 .OR. ITS.EQ.20 )      GO TO 110      533420
1      C      533430
7      ANM1 = A(NN,NM1)      533440
7      ANM1M1 = A(NM1,NM1)      533450
7      S = A(NN,NM1)*B(NM1,NM1) - ANM1M1*B(NM1,NM1)      533460
7      W = ANM1*B(NN,NN)*      533470
6      $ (A(NM1,NM1)*B(NM1,NM1) - ANM1M1*B(NM1,NM1))      533480
7      Y = (ANM1M1*B(NN,NN) - S)/2.0      533490
7      Z = CSQRT(Y*Y + W)      533500
7      IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O )      GO TO 100      533510
7      DO = REAL(Y/Z)      533520
7      IF( DO.LT.O.O )      Z = -Z      533530
3      100 CONTINUE      533540
7      DEN = (Y + Z)*B(NM1,NM1)*B(NN,NN)      533550
7      IF( REAL(DEN).EQ.O.O .AND.      533560
6      $ AIMAG(DEN).EQ.O.O )      533570
7      $DEN = CMPLX(EPSA,O.O)      533580
6      NUM = (Y + Z)*S - W      533590
7      533600
7      533610

```

PROJECT: CTJJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJJC197 PAGE: 47 OF 50

MAIN2

```

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8
7      GO TO 120
3      110 CONTINUE
7      Y = A(NM1,NM-2)
7      NUM = CMPLX(ABS(REAL(ANNM1)) + ABS(AIMAG(ANNM1)),
6      $      ABS(REAL(Y)) + ABS(AIMAG(Y)) )
7      DEN = CMPLX(1.0,0.0)
3      120 CONTINUE
7      IF( NV.EQ.L+1 ) GO TO 140
7      D1 = ABS(REAL(A(NN,NM))) + ABS(AIMAG(A(NN,NM)))
7      D2 = ABS(REAL(A(NM1,NM1))) + ABS(AIMAG(A(NM1,NM1)))
7      E1 = ABS(REAL(ANNM1)) + ABS(AIMAG(ANNM1))
7      NL = NV - (L + 1)
7      DO 130 MB=1,NL
7      M = NV - MB
7      EO = E1
7      Y = A(M,M-1)
7      E1 = ABS(REAL(Y)) + ABS(AIMAG(Y))
7      DO = D1
7      D1 = D2
7      Y = A(M-1,M-1)
7      D2 = ABS(REAL(Y)) + ABS(AIMAG(Y))
7      Y = A(M,M)*DEN - B(M,M)*NUM
7      DO = (DO + D1 + D2)*( ABS(REAL(Y)) + ABS(AIMAG(Y)) )
7      EO = EO+E1*( ABS(REAL(DEN)) + ABS(AIMAG(DEN)) ) + DO
7      IF( EO.EQ.DO ) GO TO 150
3      130 CONTINUE
3      140 CONTINUE
7      M = L
3      150 CONTINUE
7      ITS = ITS + 1
7      W = A(M,M)*DEN - B(M,M)*NUM
7      Z = A(M+1,M)*DEN
7      D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))
7      D2 = ABS(REAL(W)) + ABS(AIMAG(W))
7      LOR1 = 1
7      NNORN = N
7      DO 310 I=M,NM1
7      J = I + 1
7      IF( I.EQ.M ) GO TO 170
7      W = A(I,I-1)
7      Z = A(J,I-1)
7      D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))
7      D2 = ABS(REAL(W)) + ABS(AIMAG(W))
7      IF( D1.EQ.O.O ) GO TO 60
3      170 CONTINUE
7      IF( D2.GT.D1 ) GO TO 190
7      DO 180 K=1,NNORN
7      Y = A(I,K)
7      A(I,K) = A(J,K)
7      A(J,K) = Y
7      Y = B(I,K)
7      B(I,K) = B(J,K)
7      B(J,K) = Y
3      180 CONTINUE

```

533620
 533630
 533640
 533650
 533660
 53367
 533680
 533690
 533700
 533710
 533720
 533730
 533740
 533750
 533760
 533770
 533780
 533790
 533800
 533810
 533820
 533830
 533840
 533850
 533860
 533870
 533880
 533890
 533900
 533910
 533920
 533930
 533940
 533950
 533960
 533970
 533980
 533990
 534000
 534010
 534020
 534030
 534040
 534050
 534060
 534070
 534080
 534090
 534100
 534110
 534120
 534130
 534140
 534150

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 48 OF 50

```

7  IF( I.GT.M )      A(I,I-1) = A(J,I-1)      534160
7  IF( D2.EQ.O.O )      GO TO 220      534170
7  Y = CMPLX( REAL(W)/D1, AIMAG(W)/D1 )/      534180
6  $      CMPLX( REAL(Z)/D1, AIMAG(Z)/D1 )      534190
7  GO TO 200      534200
3  190 CONTINUE      534210
7  Y = CMPLX( REAL(Z)/D2, AIMAG(Z)/D2 )/      534220
6  $      CMPLX( REAL(W)/D2, AIMAG(W)/D2 )      534230
3  200 CONTINUE      534240
7  DO 210 K=I,NNORN      534250
7  A(J,K) = A(J,K) - Y*A(I,K)      534260
7  B(J,K) = B(J,K) - Y*B(I,K)      534270
3  210 CONTINUE      534280
3  220 CONTINUE      534290
7  IF( I.GT.M )      A(J,I-1) = CMPLX(O.O,O.O)      534300
7  Z = B(J,I)      534310
7  W = B(J,J)      534320
7  D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))      534330
7  D2 = ABS(REAL(W)) + ABS(AIMAG(W))      534340
7  IF( D1.EQ.O.O )      GO TO 60      534350
7  IF( D2.GT.D1 )      GO TO 270      534360
7  DO 230 K=LOR1,J      534370
7  Y = A(K,J)      534380
7  A(K,J) = A(K,I)      534390
7  A(K,I) = Y      534400
7  Y = B(K,J)      534410
7  B(K,J) = B(K,I)      534420
7  B(K,I) = Y      534430
3  230 CONTINUE      534440
7  IF( I.EQ.NM1 )      GO TO 240      534450
7  Y = A(J+1,J)      534460
7  A(J+1,J) = A(J+1,I)      534470
7  A(J+1,I) = Y      534480
3  240 CONTINUE      534490
7  DO 250 K=1,N      534500
7  Y = X(K,J)      534510
7  X(K,J) = X(K,I)      534520
7  X(K,I) = Y      534530
3  250 CONTINUE      534540
7  B(J,I) = CMPLX(O.O,O.O)      534550
7  IF( D2.EQ.O.O )      GO TO 310      534560
7  Z = CMPLX( REAL(W)/D1, AIMAG(W)/D1 )/      534570
6  $      CMPLX( REAL(Z)/D1, AIMAG(Z)/D1 )      534580
7  GO TO 280      534590
3  270 CONTINUE      534600
7  Z = CMPLX( REAL(Z)/D2, AIMAG(Z)/D2 )/      534610
6  $      CMPLX( REAL(W)/D2, AIMAG(W)/D2 )      534620
3  280 CONTINUE      534630
7  DO 290 K=LOR1,J      534640
7  A(K,I) = A(K,I) - Z*A(K,J)      534650
7  B(K,I) = B(K,I) - Z*B(K,J)      534660
3  290 CONTINUE      53467
7  B(J,I) = CMPLX(O.O,O.O)      534680
7  IF( I.LT.NM1 )      A(I+2,I) = A(I+2,I) - Z*A(I+2,J)      534690
7

```

PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24
 GROUP: STB1 LEVEL: 01.00 TIME: 12:02
 TYPE: FORT USERID: CTJC197 PAGE: 49 OF 50

START

```

COL 1-----2-----3-----4-----5-----6-----7-----8
7   DO 300 K=1,N
7   X(K,I) = X(K,I) - Z*X(K,J)
3   300 CONTINUE
3   310 CONTINUE
7   GO TO 60
3   320 CONTINUE
7   EIGA(NN) = A(NN,NN)
7   EIGB(NN) = B(NN,NN)
7   IF( NN.EQ.1 ) GO TO 330
7   ITER(NN) = ITS
7   NN = NN1
7   IF( NN.GT.1 ) GO TO 50
7   ITER(1) = 0
7   GO TO 320
3   330 CONTINUE
7   M = N
3   340 CONTINUE
7   ALFM = A(M,M)
7   BETM = B(M,M)
7   B(M,M) = CMPLX(1.0,0.0)
7   L = M - 1
7   IF( L.EQ.0 ) GO TO 370
3   350 CONTINUE
7   L1 = L + 1
7   SL = CMPLX(0.0,0.0)
7   DO 360 J=L1,M
7   SL = SL + B(J,M)*(BETM*A(L,J) - ALFM*B(L,J))
3   360 CONTINUE
7   Y = BETM*A(L,L) - ALFM*B(L,L)
7   IF( REAL(Y).EQ.0.0 .AND.
6   $ AIMAG(Y).EQ.0.0 )
6   $ Y = CMPLX( (EPSA+EPSB)/2.0, 0.0 )
7   B(L,M) = -SL/Y
7   L = L - 1
3   370 CONTINUE
7   IF( L.GT.0 ) GO TO 350
7   M = M - 1
7   IF( M.GT.0 ) GO TO 340
7   M = N
3   380 CONTINUE
7   DO 400 I=1,N
7   S = CMPLX(0.0,0.0)
7   DO 390 J=1,M
7   S = S + X(I,J)*B(J,M)
3   390 CONTINUE
7   X(I,M) = S
3   400 CONTINUE
7   M = M - 1
7   IF( M.GT.0 ) GO TO 380
7   M = N
3   410 CONTINUE
7   SS = 0.0
7   DO 420 I=1,N
7   R = ABS(REAL(X(I,M))) + ABS(AIMAG(X(I,M)))
7

```

534700
 534710
 534720
 534730
 534740
 534750
 534760
 534770
 534780
 534790
 534800
 534810
 534820
 534830
 534840
 534850
 534860
 534870
 534880
 534890
 534900
 534910
 534920
 534930
 534940
 534950
 534960
 534970
 534980
 534990
 535000
 535010
 535020
 535030
 535040
 535050
 535060
 535070
 535080
 535090
 535100
 535110
 535120
 535130
 535140
 535150
 535160
 535170
 535180
 535190
 535200
 535210
 535220
 535230

